

Microstructural Evolution and Oxidation Behavior of T91/T92 Steel upon Long-Term Steam Test

K. Shin¹, H.Y. Ma¹ and Y.S. He¹, S.Y. Bae²

¹ School of Nano and Advanced Material Engineering, Changwon National University, Changwon 51140, Korea

² Advanced Materials Group, Korea Electric Power Company, Daejeon 305308, Korea

Heat resistant steel is heavily used for boiler system for highly efficient power generation, which is mostly operated in supercritical steam environment (~566°C). Therefore, the high temperature oxidation mechanism of heat resistant steel is that of high interest for understanding and deterring of the premature failure of the boiler parts [1]. Thus, the detailed characterization, i.e., qualitative analysis and quantification microstructural elements such as formation and thickness of corrosion layers and data collection, pertaining to the oxidation behavior upon the usage of such heat resistant steel is a key for maintenance, lifetime extension, and achievement of efficiency improvement of power generation.

In this study, T91 and T92 steels were steam tested at the supercritical condition, i.e., at 600°C, 650°C and 700°C, for 10000, 15000, and 20,000 h. SEM/EDS, EBSD and TEM were used for microstructural analysis of the oxide layer, i.e., morphology, chemical composition, phase distributions and evolution.

Typical SEM/EBSD analysis of T91 and T92 were shown in Figure 1 and Figure 2. The oxide layer formed on the none-treated surface consisted of an outer layer of iron oxide (Fe₂O₃ and Fe₃O₄) and inner layer of chromium oxide (FeCr₂O₄ and Cr₂O₃) on the specimen. Flaking of the iron oxide scale layer was related to coarsening of Fe₃O₄ layer in the specimens. The oxidation sequences of T91/T92 under steam environment are: 1) formation of iron oxide out layer and chromium oxide inner layer, 2) growth of Fe₃O₄ in iron oxide layer and spallation of iron oxide layer, 3) growth of iron chromium layer and re-formation of iron oxide outer layer. Cr depletion zones were present below the oxide layer in both specimens, formation of which was attributed to the formation of Cr rich layer.

Cr₂₃C₆ in T91 and Laves phase in T92 specimen were found after the steam test, which were distributed along grain boundaries. Surface grain coarsening (over 20 μm) occurred below oxide layer in T91 specimen (5.1 μm in matrix) (Figure 1b), which was attributed to the dissolution of Cr₂₃C₆ at the surface region. However, no grain coarsening occurred in T92 for the high stabilization and pinning effect on grain boundaries by Laves phase.

T92 showed better corrosion resistance than that of the T91. Dissolution of Cr₂₃C₆ and surface grain coarsening led to the decomposition of Cr-rich layer, which reduced the corrosion resistance of T91 specimen.

References:

[1] L. Tan, X. Ren and T.R. Allen, Corrosion Science 52 (2010) p.1520.

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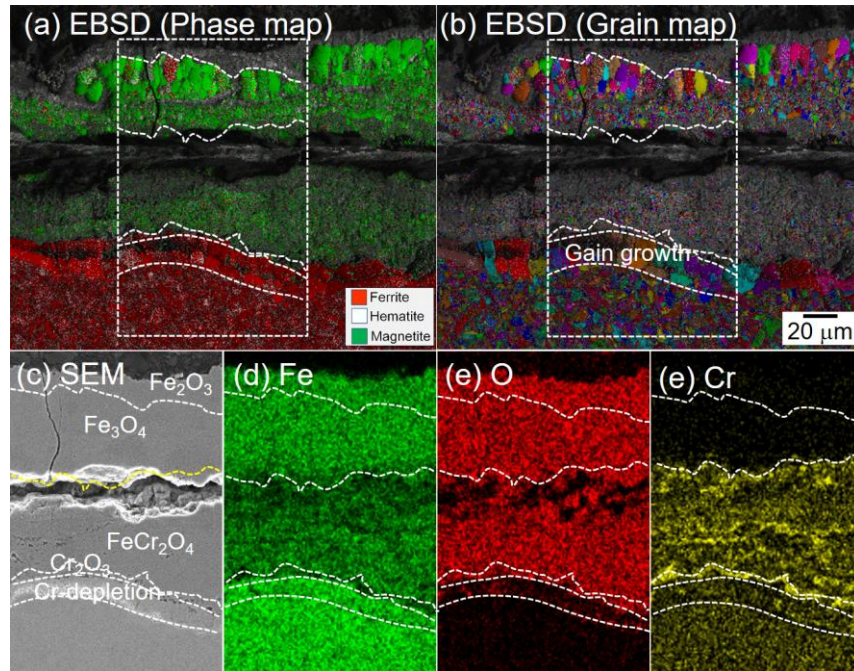


Figure 1. (a) EBSD phase mapping, (b) EBSD grain mapping, (c) SEM, (d) BSE, and (e~g) EDS elemental mapping of the steam tested T91 specimen at 650°C for 10,000 h.

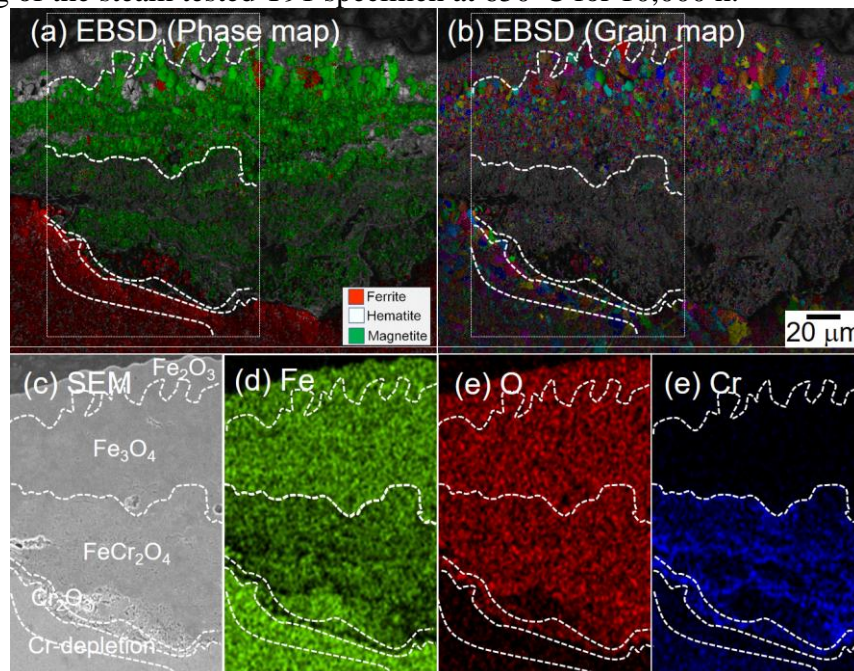


Figure 2. (a) EBSD phase mapping, (b) EBSD grain mapping, (c) SEM, (d) BSE, and (e~g) EDS elemental mapping of the steam tested T92 specimen at 650°C for 10,000 h.