



Onset of convection cells in a horizontally rotating cylinder partially filled with liquid

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We investigate flow of liquid which is partially filled in a cylindrical container horizontally rotating about its axis of symmetry. Even if the rotation is slow enough to keep the liquid–gas interface almost undeformed, convection cells whose circulation axis is perpendicular to the container’s rotational axis can be sustained. We conduct experiments by particle image velocimetry and direct numerical simulations with the S-CLSVOF and immersed boundary methods to reveal the condition of the Reynolds number, the aspect ratio of the container and the filling ratio of liquid for the onset of these convection cells. When the filling ratio is not too large, as the Reynolds number increases, convection cells appear through a pitchfork bifurcation in an infinitely long cylinder. This bifurcation becomes imperfect in the case of a finite-length cylinder. In contrast, when the filling ratio is large enough, convection cells appear through a subcritical bifurcation. Through these investigations, it becomes evident that the axial wavelength of sustained convection cells is an increasing function of the filling ratio in an infinitely long cylinder. In practice, to sustain intense convection cells, we should use a cylinder with the length equal to an integer multiple of the wavelength of the most unstable mode in the infinite-length cylinder. Although we focus on the liquid-pool regime with small Froude numbers, the critical Reynolds number for the pitchfork bifurcation weakly depends on the Froude number. This dependence is explained by considering the changes in the effective filling ratio and the convection velocity.

Key words: gas/liquid flow

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1. Introduction

Single-phase flow in a cylindrical container rotating about its axis of symmetry at a constant angular velocity always tends to the solid-body rotation, and therefore axial flow is never sustained. In contrast, multi-phase flow in a rotating cylinder exhibits a surprisingly wide variety of states; see Seiden & Thomas (2011). For example, when we suspend small solid particles in the fluid filled in a container, inertial waves are excited, which lead to a periodic pattern of particle distribution (Lipson 2001; Seiden, Ungarish & Lipson 2005). When liquid is partially filled in the cylindrical container, i.e. when there coexist gas and liquid, flow states can be highly non-trivial and the flow is sometimes accompanied with axial flow. It is such non-trivial flow of liquid partially filled in a rotating cylinder (figure 1) that is the target of the present study. Here, we restrict ourselves to the case where the cylinder rotates horizontally about its axis of symmetry.

Since this flow system is ubiquitous, numerous authors investigated it, in particular, in the regime where a container rapidly rotates. In such a case, fluid forms a film on the wall of the container. This rimming flow is not only scientifically interesting, but also important in engineering applications such as paper manufacturing (Pereira, Valenzuela & Valenzuela 2010; Ghosh 2011; Hubbe 2021; Majeed *et al.* 2022), evaporators (Willems *et al.* 2010; Chatterjee, Sugilal & Prabhu 2019), centrifugal thernit process (Menekse, Wood & Riley 2006), centrifugal casting process (Keerthiprasad *et al.* 2011; Boháček *et al.* 2015) and triboelectric nanogenerators (Kim *et al.* 2016). In fact, flow characteristics such as the instability of the rimming flow were extensively investigated experimentally, theoretically and numerically (Phillips 1960; Yih 1960; Johnson 1988; Thoroddsen & Mahadevan 1997; Hosoi & Mahadevan 1999; Tirumkudulu & Acrivos 2001; Ashmore, Hosoi & Stone 2003; Benilov, Benilov & Kopteva 2008; Kozlov & Polezhaev 2015; Kakimpa, Morvan & Hibberd 2016; Nicholson *et al.* 2019; Sadeghi, Diosady & Blais 2022).

When the rotation of the container is not fast enough to form the rimming flow, a stationary pool of liquid exists at the bottom of the cylinder. We emphasize that flow can be non-trivial even in this regime. More concretely, under some circumstances, flow of partially filled liquid is accompanied by axial motion. The seminal experiments in this flow regime were conducted by Balmer (1970), who discovered a periodic, in the axial direction, liquid column. Since then, many experimental and theoretical studies revealed patterns of the liquid–gas interface in a rotating cylinder (Benjamin & Pathak 1987; Melo 1993; Thoroddsen & Mahadevan 1997; Thoroddsen & Tan 2004; Chen *et al.* 2007). One of the most interesting interface patterns observed in this flow is the shark-teeth-like pattern (Thoroddsen & Mahadevan 1997). Thoroddsen & Tan (2004) visualized flow by using small bubbles as tracers to discover counter-rotating pairs of convection cells, whose axes were perpendicular to the rotation axis of the container. They concluded that the creation of the shark-teeth-shaped interface was relevant to the formation of the convection cells.

We emphasize that the flow sustained in the case with even slower rotations, where the liquid–gas interface is hardly deformed, is still interesting, although only a few authors investigated this regime. The most fascinating phenomenon in this regime is the emergence of the convection cells, whose axis is perpendicular to the rotational axis of the cylinder. Romanò, Hajisharifi & Kuhlmann (2017) first numerically demonstrated this phenomenon. Though observed convection cells remind us of those in the experiments by Thoroddsen & Tan (2004), we note that the slip boundary condition was imposed on the undeformable liquid–gas interface in the numerical simulations by Romanò *et al.* (2017). They showed that when the Reynolds number $Re = \omega R^2/\nu$, where ω is the angular velocity, R is the container radius and ν is the kinematic viscosity of liquid, satisfied the condition

Convection cells in a horizontally rotating cylinder

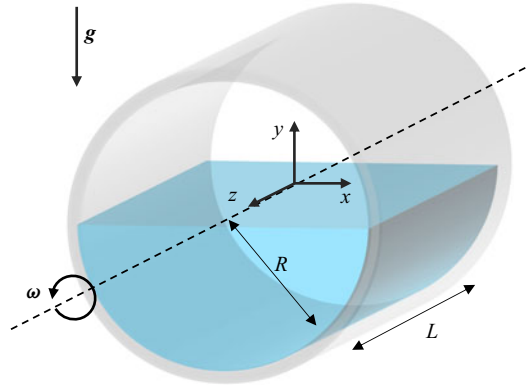


Figure 1. Schematic of a horizontally rotating cylinder with a liquid–gas interface and the definition of the coordinate system whose origin is set at the centre of the cylinder. We define R , L and $\omega = (0, 0, \omega)$ as the radius, length and angular velocity of the cylinder, and $\mathbf{g} = (0, -g, 0)$ as the gravitational acceleration.

$Re > 820 \pm 50$, the convection cells could be sustained in the case that the filling ratio, which is defined as the ratio of liquid volume to the container volume, is $\Psi \approx 0.05$.

Romanò *et al.* (2017) also demonstrated that the convection cells sustained in the pool at the bottom of the container were relevant to liquid mixing. Since counter-rotating pairs of convection cells enhance the stretch and fold of fluid elements, they lead to effective mixing in the liquid phase. This implies that this simple flow system can serve as a bladeless mixer, which is advantageous because we do not need to clean-up blades and because it can avoid damage to delicate materials. This is why many kinds of bladeless mixers were proposed even recently (Goto, Shimizu & Kawahara 2014; Meunier 2020; Watanabe & Goto 2022; Goto *et al.* 2023). Since the current system is the simplest possible, we expect its wide applications in many fields. Therefore, it is crucial from not only scientific but also engineering viewpoints to reveal the condition that the convection cells are sustained.

Since Romanò *et al.* (2017) showed the critical Reynolds number Re_c for the onset of the convection cells only for a single condition of the filling ratio, the filling-rate dependence of Re_c is unknown. Furthermore, since their numerical simulation neglects the deformation of the liquid–gas interface, the effect of the deformation on Re_c is also unknown. We also emphasize that although the present system can be categorized in the same group as the Taylor–Couette flow and Rayleigh–Bénard convection, its understanding is poor in contrast to these flows, for which the phase diagram, bifurcations, instability, flow dynamics and so on were extensively examined by many authors. In other words, the present study is one of the first steps to understand this canonical flow.

Thus, the main purpose of this study is to reveal the condition under which the convection cells of partially filled liquid are sustained in the rotating cylinder. As will be described in detail in the following sections, the critical Reynolds number Re_c depends on the flow conditions such as the filling ratio Ψ and the Froude number Fr as well as the aspect ratio of the container. In the present study, we determine the critical parameters as accurate as possible and we also develop related arguments on bifurcation structures depending on Ψ . To this end, we conduct both laboratory experiments and direct numerical simulation (DNS). Though experiments are advantageous to discover phenomena, they are sometimes disadvantageous for a systematic parametric survey. This is particularly the case when we consider flow with a liquid–gas interface because it depends both on the Reynolds and Froude numbers; it is impossible to change the former with fixing the latter

with the same container and working fluid in experiments. Therefore, we use DNS for the parametric survey. We emphasize that accurate DNS of flow with a free interface is still difficult, although many authors (Keerthiprasad *et al.* 2011; Dawedeit *et al.* 2012; McBride *et al.* 2013; Boháček *et al.* 2015; Majeed *et al.* 2022; Sadeghi *et al.* 2022) already conducted DNS of flow with significant deformations of the liquid–gas interface in the rimming flow. Thus, in the present study, we implement state-of-the-art numerical schemes (Yokoi 2007; Albadawi *et al.* 2013; De Vita *et al.* 2021) of multi-phase flow to conduct DNS, which we carefully validate by using experimental data.

2. Method

2.1. Configuration and control parameters

Figure 1 shows the configuration of the examined system, where we drive flow in a cylindrical container with radius R and axial length L by rotating it at constant angular velocity ω about its horizontal axis. We partially fill the container with a liquid with density ρ_l and viscosity μ_l . We denote the filling ratio of the liquid by Ψ . We also denote the density and viscosity of gas in the container by ρ_g and μ_g , respectively.

We define Cartesian coordinate (x, y, z) as shown in figure 1, where the gravitational acceleration \mathbf{g} is expressed as $(0, -g, 0)$ and the angular velocity $\boldsymbol{\omega}$ of the cylinder as $(0, 0, \omega)$.

Let us summarize the control parameters of the present system. First, the dimensionless length $L^* = L/R$ of the container normalized by R and the filling ratio Ψ of the liquid are important parameters. Once we fix L^* and Ψ , the flow state depends on the viscous force, inertial force, gravitational force and surface tension. Hence, three control parameters are expressed by the ratios between these forces. Though there are several choices of the three control parameters, we often employ the Reynolds number,

$$Re = \frac{\rho_l R^2 \omega}{\mu_l}, \quad (2.1)$$

which is the ratio between the inertial and viscous forces, the Froude number,

$$Fr = \frac{R\omega^2}{g}, \quad (2.2)$$

which is the ratio between the inertial and gravitational forces, and the Bond number,

$$Bo = \frac{g\rho_l R^2}{\Psi\sigma}, \quad (2.3)$$

which is the ratio between the gravitational force and the force due to the surface tension. Here, σ denotes the surface tension of liquid. Note that we have adopted the definition of Bo similar to previous studies (Ashmore *et al.* 2003; Sadeghi *et al.* 2022).

In the present study, we restrict ourselves to the cases where the inertial force is much larger than the viscous force; namely, $Re \gg 1$. However, since the main target is the bifurcation of steady flow, the turbulence regime is beyond the scope of this study. Therefore, we examine the cases with relatively small Reynolds numbers, $Re \lesssim O(10^2)$.

We also restrict ourselves to the cases where the liquid–gas interface is hardly deformed because the gravitational effect dominates the inertial force and surface tension. More

concretely, we examine the cases with $Fr \lesssim 0.1$ for which the inertial force cannot overcome the gravitational force to deform the liquid–gas interface. In all the examined cases, Bo is much larger than 1 so that we can neglect the effects of surface tension.

Sometimes the flow regimes are classified by the gravitational parameter (Ashmore *et al.* 2003),

$$\Lambda = \frac{\Psi^2 Re}{Fr}, \tag{2.4}$$

which denotes the ratio between the gravitational force and the viscous force because it can be rewritten as $(\rho\delta g)/(\mu(R\omega/\delta))$, where $\delta (\approx \Psi R)$ is the thickness of the uniform liquid film for $\Psi \ll 1$. The flow is classified into three regimes in terms of Λ (the shear-dominated regime for $\Lambda \leq 2$, the transitional regime for $2 < \Lambda \leq 5$ and the gravitational-dominated regime for $\Lambda > 5$). In the first regime, a coating flow with a nearly uniform liquid film is formed, while the last regime is often called the liquid-pool regime because a stationary pool of liquid is formed at the bottom of the cylinder. Since we examine the cases with small Fr , large Re and not so low Ψ , Λ is much larger than 1. Therefore, according to the classification in terms of Λ , we deal with the liquid-pool regime.

In summary, the main purpose of the present study is to reveal the conditions of L^* , Ψ and Re for the convection cells to appear for sufficiently large Bo (i.e. surface tension is negligible) and sufficiently small Fr (i.e. the liquid–gas interface is hardly deformed). In § 5.3, we will also briefly examine the effect of Fr on flow states.

In experiments, we have to design the set-up so that we can capture the critical Reynolds number Re_c for the onset of convection cells, which is, as will be shown below, $O(10^2)$. First, as for the size of the experimental apparatus, we use a cylindrical container with radius $R = O(10^{-1})$ m. Then, to satisfy the condition $Bo \gg 1$, we may use either water ($\sigma = 0.071$ N m⁻¹) or silicone oil (0.0208 N m⁻¹) as a working fluid. To satisfy the condition that $Re = O(10^2)$, we must set the angular velocity of the container as $\omega \approx 10^4 \mu_l / \rho_l$. However, if ω is too small, it is difficult to accurately set the angular velocity with the stepper motor (see figure 2), and tracer particles for visualizations and measurements can settle. Therefore, we use silicone oil, rather than water, with a kinematic viscosity of $\mu_l / \rho_l \approx 50$ cSt so that we can set the angular velocity at $\omega (\approx 1$ rps). In this experimental set-up, Fr is $O(10^{-2})$ and therefore the liquid–gas interface is undeformed to keep an almost horizontal flat surface. For DNS, we can set the parameters arbitrarily. For simplicity, however, we ignore the surface tension as well as the wettability in DNS.

When we show results in non-dimensional forms, we use the time and length units of ω^{-1} and R , respectively. Non-dimensional time, length and velocity are denoted with superscript *.

2.2. Experimental method

Figure 2(a) shows the schematic of the experimental apparatus. We rotate a cylindrical container with $R = 50$ mm about the horizontal axis. Though we can set containers with different lengths, in the following, we show results with a relatively long cylinder; namely, $L = 800$ mm, therefore, $L^* = L/R = 16$. The container is made of acrylic with thickness 10 mm. We drive the rotation by a stepper motor (Oriental Motor, ARM66AC-PS10) with the step angle 0.036° and a pulse generator (Raspberry Pi 4 model B). The rotation axis precisely coincides with the axis of the cylinder.

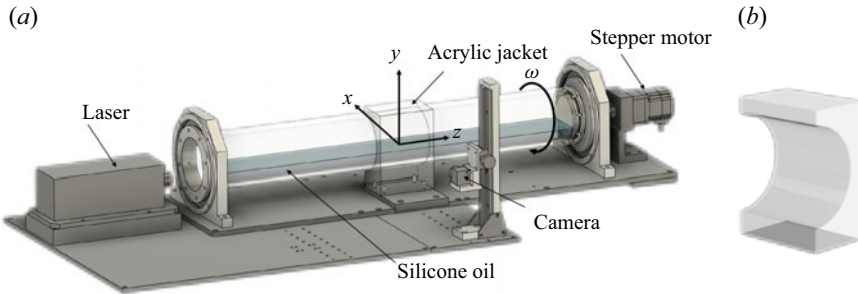


Figure 2. (a) Schematic of the experimental apparatus. The acrylic cylindrical container ($R = 50$ mm, $L = 800$ mm, thickness 10 mm) rotates about the horizontal axis of symmetry at constant angular velocity ω . The container is partially filled with silicone oil. We observe flow visualized by a laser sheet on the vertical plane. (b) Acrylic jacket to reduce the refraction between the container and air.

As mentioned in the previous subsection, we use silicone oil (Shin-Etsu Silicone, KF96-50cs) as the working fluid. We control the room temperature so that the fluid temperature during experiments is 25.0 ± 0.3 °C. We measure the viscosity of the silicone oil by the viscometer (Kokugo, TVB-10M) and the mass density as 0.0478 Pa s and 955 kg m $^{-3}$, respectively. Therefore, the kinematic viscosity is estimated as 50.1 mm 2 s $^{-1}$. Since the surface tension of the silicone oil is $\sigma = 0.0208$ N m $^{-1}$, the Bond number is $Bo \approx 1.1 \times 10^3$ for $\Psi = 1$, which is large enough to neglect the effects of the surface tension. Since we experimentally examine the cases with $\Psi = 0.2$ and 0.4 , 0.5π rad s $^{-1} \leq \omega \leq 1.8\pi$ rad s $^{-1}$, Λ is always sufficiently large; for example, $\Lambda \approx 69$ for $\Psi = 0.2$ and $\omega = 1.8\pi$ rad s $^{-1}$.

We seed nylon powder with diameter and density of approximately 50 μ m and 1.02 g cm $^{-3}$, respectively, for a volume fraction of approximately 40 ppm and use a continuous laser sheet (Kanomax, CW532-2W, wavelength 532 nm, power 750 mW, width approximately 1.5 mm) on the vertical plane through the horizontal axis to visualize and measure by particle image velocimetry (PIV) the flow on the plane. For the visualization and PIV, we use an acrylic jacket (figure 2b) which is set along the cylindrical container with a clearance of approximately 1 mm. By using this jacket, we can drastically reduce the distortion due to the index mismatch of the acrylic container and air.

The method of flow visualization is as follows. We take images with a digital camera (Nikon, D7100, lens AI Nikkor 20 mm $f/2.8S$). We use a long exposure time, which is comparable to the spin period of the container, to record the pathlines of flow on the vertical plane. We take, in addition to images of the entire flow, close-up images through the acrylic jacket (figure 2b).

For PIV, we use a digital camera (Ditect, HAS-02M, resolution 1024×1280 pixels, frame rate 100 fps) with a lens (Fujinon, DF6HA-1B 6 mm $f/1.2$). To determine the onset of the convection cells in the central region of the cylindrical container, we only record images of the region 128×160 mm through the jacket (figure 2b). We use the direct correlation method, where we set the interrogation window of size 24×24 pixels to estimate the correlation function. We employ a sub-pixel analysis under the assumption that the correlation function has a normal form. We record the time series of images for 10 revolutions.

Both flow visualizations and PIV are conducted in the steady state after a transient time, approximately 30 revolutions, when we change flow conditions.

2.3. Numerical method

We numerically solve the two-phase Navier–Stokes equation,

$$\rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = -\nabla p + \nabla \cdot (\mu \mathbf{D}(\mathbf{u})) + \rho \mathbf{g} + \rho \mathbf{f}, \quad (2.5)$$

and the mass conservation equation,

$$\nabla \cdot \mathbf{u} = 0, \quad (2.6)$$

to simulate flow in the cylinder (figure 1). Here, $\mathbf{u} = (u, v, w)$ is the velocity, p is the pressure and $\mathbf{D}(\mathbf{u}) = \nabla \mathbf{u} + (\nabla \mathbf{u})^T$. Note that the density ρ and viscosity μ of the fluid (i.e. liquid and gas) are determined by the expression (2.11a,b) explained below. The interaction force \mathbf{f} between the fluid and solid is estimated by

$$\mathbf{f} = \chi \frac{U_f - \mathbf{u}}{\delta t}, \quad (2.7)$$

where χ is the volume fraction of the solid, U_f is the velocity of the solid and δt is the numerical time step (Kajishima *et al.* 2001). This method was used, for example, to successfully represent a pipe wall to simulate turbulent flow in it (Ardekani *et al.* 2018). We set the cylindrical shell with wall thickness 12Δ , where Δ is the numerical grid width in the x direction. Note that we set a uniform orthogonal grid, whose width depends on the direction, in a rectangular computational domain. Then, substituting $U_f = -\omega y \mathbf{e}_x + \omega x \mathbf{e}_y$ into (2.7), we determine \mathbf{f} in the domain. Here, \mathbf{e}_x and \mathbf{e}_y are the unit vectors in the x and y directions, respectively.

To capture the motion of the liquid–gas interface, we use a simple coupled volume of fluid with the level-set (S-CLSVOF) method (Albadawi *et al.* 2013), which is a combination of the volume of fluid method (Hirt & Nichols 1981) and level-set method (Sussman, Smereka & Osher 1994). Here, we briefly explain this method. First, we solve the advection equation of the volume fraction ϕ_l of liquid,

$$\frac{\partial \phi_l}{\partial t} + (\mathbf{u} \cdot \nabla) \phi_l = 0, \quad (2.8)$$

by the THINC/WLIC method (Yokoi 2007). To impose the Neumann boundary condition for ϕ_l on the wall and to set the contact angle as 90° , we employ the method used in the previous studies (Sussman 2001; Yokoi 2013; Sun & Sakai 2016). Second, we set the initial state ψ_0 of the level-set function by $0.75(2\phi_l - 1)\Delta$ (Albadawi *et al.* 2013). We then reinitialize the level-set function ψ by the scheme proposed by Sussman *et al.* (1994). In the scheme, we integrate

$$\frac{\partial \psi}{\partial t'} = \frac{\psi_0}{\sqrt{\psi_0^2 + \Delta^2}} (1 - |\nabla \psi|) \quad (2.9)$$

to obtain the reconstructed ψ as the steady solution of (2.9). Here, t' is an artificial time. We conduct this operation at each time step.

We use the level-set function ψ to define the physical properties of the fluid. The density ρ and viscosity μ are expressed in terms of a smooth Heaviside function,

$$H(\psi) = \begin{cases} 0 & (\psi < -\varepsilon), \\ (\psi + \varepsilon)/2\varepsilon + \sin(\pi\psi/\varepsilon)/2\pi & (|\psi| \leq \varepsilon), \\ 1 & (\psi > \varepsilon), \end{cases} \quad (2.10)$$

where $\varepsilon = 1.5\Delta$. Then, we estimate ρ and μ by

$$\rho = H(\psi)\rho_l + (1 - H(\psi))\rho_g \quad \text{and} \quad \mu = H(\psi)\mu_l + (1 - H(\psi))\mu_g, \quad (2.11a,b)$$

respectively.

We use finite difference spatial discretization on the staggered grid. The advection term in (2.5) is expressed by the QUICK method and the other terms are handled by the second-order central difference method. We numerically integrate (2.5) and (2.6) using the SMAC method. For the advection term in (2.5), we use the second-order Adams–Bashforth method, while for the viscous term in (2.5), we use the second-order Crank–Nicolson method modified for two-phase flow (Dodd & Ferrante 2014). We employ the first-order Euler method for the remaining terms. The discretized form of the Poisson equation for pseudo-pressure is solved using the direct method with the fast Fourier transform (Dodd & Ferrante 2014; Frantzis & Grigoriadis 2019; De Vita *et al.* 2021). The Helmholtz equation for the implicit integration of the viscous term is solved iteratively using the SOR method.

In our numerical method, unphysical volume-fraction transfer to the solid region can slightly occur. Since, in some cases, we need more than 100 revolutions of the container to obtain a steady state, we cannot ignore the change in the total volume of the liquid. To overcome this problem, we slightly modify the location of the liquid–gas interface at each time step. First, we integrate the smoothed delta function calculated by

$$\delta_\varepsilon = \begin{cases} \frac{1}{2\varepsilon} \left[1 + \cos\left(\frac{\pi\psi}{\varepsilon}\right) \right] & |\psi| \leq \varepsilon, \\ 0 & |\psi| > \varepsilon \end{cases}, \quad (2.12)$$

to estimate the area S of the liquid–gas interface. Then, we advect the interface by the pseudo-velocity $\mathbf{u}_s = \nabla\psi\delta\phi_l/S\delta t$ to maintain the total volume of the liquid in the container. Here, $\delta\phi_l$ is the difference between the initial and current liquid volumes in the container. In fact, since we deal with the regime where the liquid–gas interface is hardly deformed, the normal direction of the interface $\nabla\psi$ is almost in the y direction. Therefore, we set $\mathbf{u}_s \approx (0, \delta\phi_l/S\delta t, 0)$ to the advection velocity of (2.8). We have confirmed that the deviation ratio of the total volume of the liquid in the container is less than 0.01% during the numerical integration of flow. Note that we cannot use this method with large deformations of the interface.

For numerical stability, we set the viscosity and density of gas to 1/100 of the liquid. We use the adaptive time step (Frantzis & Grigoriadis 2019) for the integration; namely, we determine δt according to the Courant–Friedrichs–Lewy (CFL) condition. Specifically, we set the time increment $\delta t = Co\Delta/u_{max}$ at each time step, where Co is the Courant number and u_{max} is the maximum velocity in the computational domain. We set $Co = 0.1$ except for the case with $Fr = 2.26 \times 10^{-3}$ in Run 7 shown in table 2.

Convection cells in a horizontally rotating cylinder

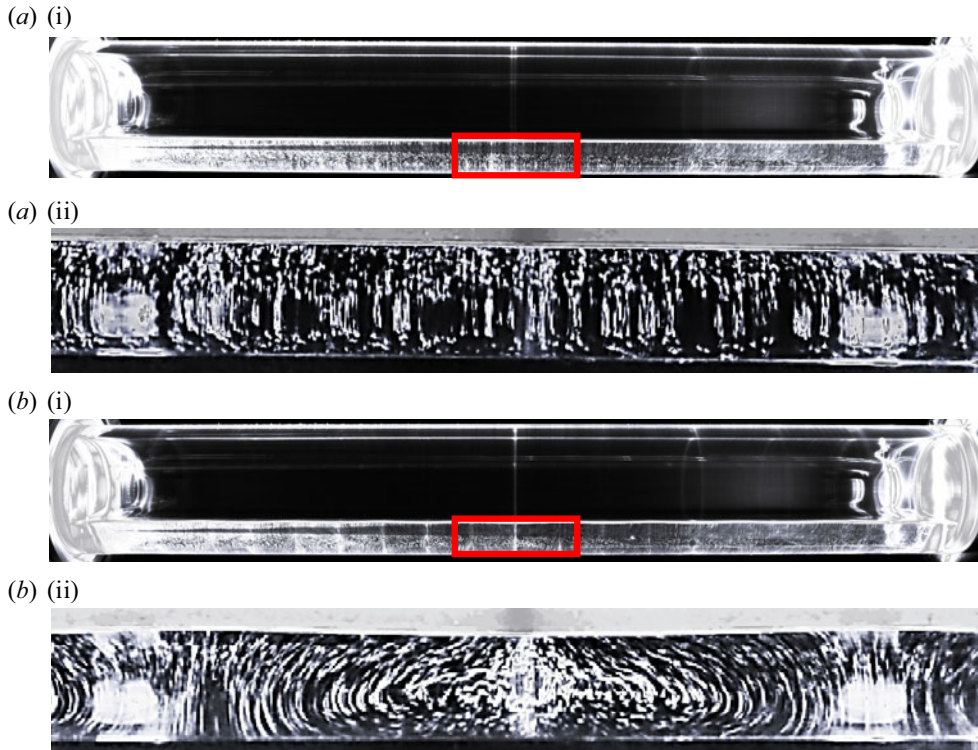


Figure 3. Visualization of pathlines on $x = 0$ plane at $\Psi = 0.2$. The angular velocities are (a) π and (b) $1.8\pi \text{ rad s}^{-1}$. We depict (ai and bi) the entire and (a(ii) and b(ii)) a part of the cylindrical container enclosed by the red rectangle in (ai and bi). In (a(ii) and b(ii)), we observe flow through the jacket shown in figure 2(b).

3. Experimental results

3.1. Visualization

As mentioned in § 1, convection cells circulating perpendicular to the rotational axis of the container appear in the cylinder. First, we experimentally demonstrate this phenomenon by flow visualizations. We examine two cases with the filling ratio Ψ being 0.2 (figure 3) and 0.4 (figure 4), for each of which we change the container's angular velocity ω . Note that Fr changes with Re , since we use the same liquid and container in all the cases. In these figures, panels (ai) and (bi) show the entire flow in the container and panels (a(ii) and (b(ii)) show the flow in a central region of the container which is visualized through the acrylic jacket (figure 2b).

We do not observe convection cells in the central region for small ω (figures 3a and 4a), while we observe them for larger ω (figures 3b and 4b). As will be shown by DNS in § 4.3, the convection cells appear through a supercritical pitchfork bifurcation, and the critical angular velocity ω_c depends on the filling ratio Ψ . In fact, these visualizations (figures 3 and 4) show that ω_c depends on Ψ . More precisely, ω_c (and the corresponding Reynolds number Re_c) for $\Psi = 0.2$ and 0.4 falls within the ranges $\pi \text{ rad s}^{-1} < \omega_c < 1.8\pi \text{ rad s}^{-1}$ ($157 < Re_c < 282$) and $0.6\pi \text{ rad s}^{-1} < \omega_c < \pi \text{ rad s}^{-1}$ ($94 < Re_c < 157$), respectively.

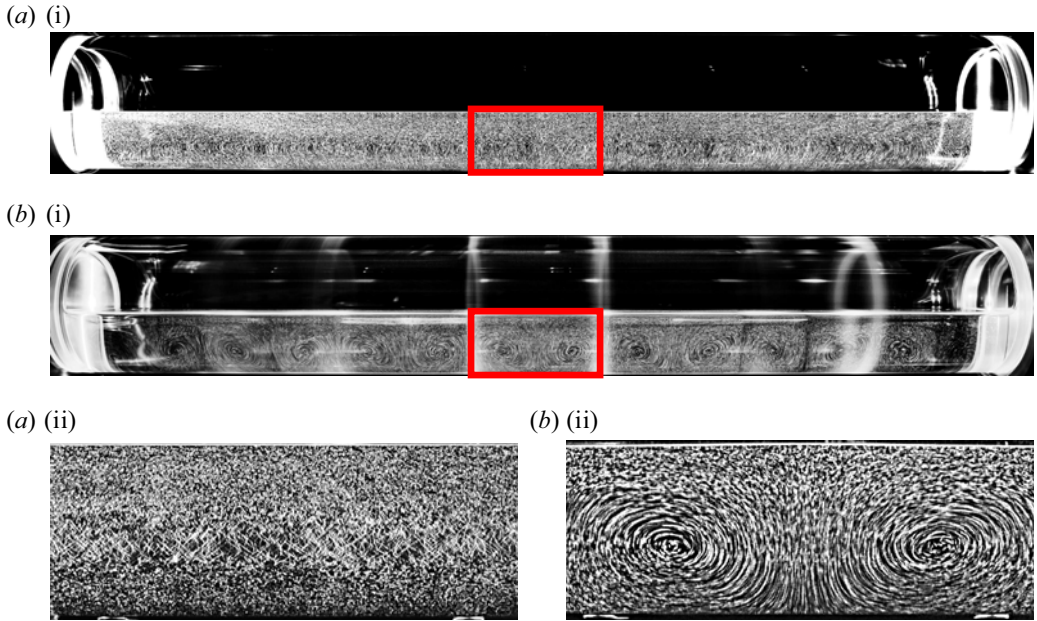


Figure 4. Similar to figure 3, but for $\Psi = 0.4$. The angular velocities are (a) 0.6π and (b) π rad s^{-1} .

3.2. PIV

Since we cannot accurately determine ω_c (and Re_c) only from the visualizations (figures 3 and 4), we quantify the intensity of convection cells using PIV to clarify their onset condition. For this PIV, to avoid the influence of refraction on the air–acrylic-jacket interface and reflection on the liquid–gas interface, we only analyse the bulk of the liquid phase ($-0.8 < y^* < h_0^* - 0.05$). Here, h_0^* is the normalized height of the liquid–gas interface without the rotation.

First, we show in figure 5 the mean flow on the $x = 0$ plane, which is obtained by the temporal average over ten revolutions of the container. For $\Psi = 0.2$, we do not observe convection cells at $\omega = 1.3\pi$ rad s^{-1} , i.e. $Re = 204$ and $Fr = 0.085$ (figure 5a), whereas they are visible at $\omega = 1.73\pi$ rad s^{-1} , i.e. $Re = 272$ and $Fr = 0.151$ (figure 5b). For $\Psi = 0.4$, similarly to $\Psi = 0.2$, we observe no convection cells when the angular velocity is smaller ($\omega = 0.7\pi$ rad s^{-1} , i.e. $Re = 110$ and $Fr = 0.0246$ in figure 5c), while they can be observed at the larger angular velocity ($\omega = 0.8\pi$ rad s^{-1} , i.e. $Re = 126$ and $Fr = 0.0322$ in figure 5d). To clarify the flow transition, we define an indicator,

$$V^* = \max[|v^*(0, y^*, z_0^*)|], \quad (3.1)$$

where z_0^* is the location of the maximum downward velocity i.e. $z_0^* = 0.75$ for $\Psi = 0.2$ and $z_0^* = 0$ for $\Psi = 0.4$. We plot V^* as a function of Re in figure 6. We observe that V^* increases significantly above a certain value of Re , which is approximately 200 for $\Psi = 0.2$ and approximately 110 for $\Psi = 0.4$. As will be shown by DNS in § 4.3, the convection cells appear through a pitchfork bifurcation. However, the experimental results shown in figure 6 seem different from this bifurcation; namely, the functional form of V^* does not obey $V^* \propto (Re - Re_c)^{1/2}$ for a pitchfork bifurcation (Strogatz 2018, § 3.4). This is due to two reasons. One is the effect of the end walls. The discussion in § 5.2 will show that the end wall makes the pitchfork bifurcation imperfect, which explains the continuous increase

Convection cells in a horizontally rotating cylinder

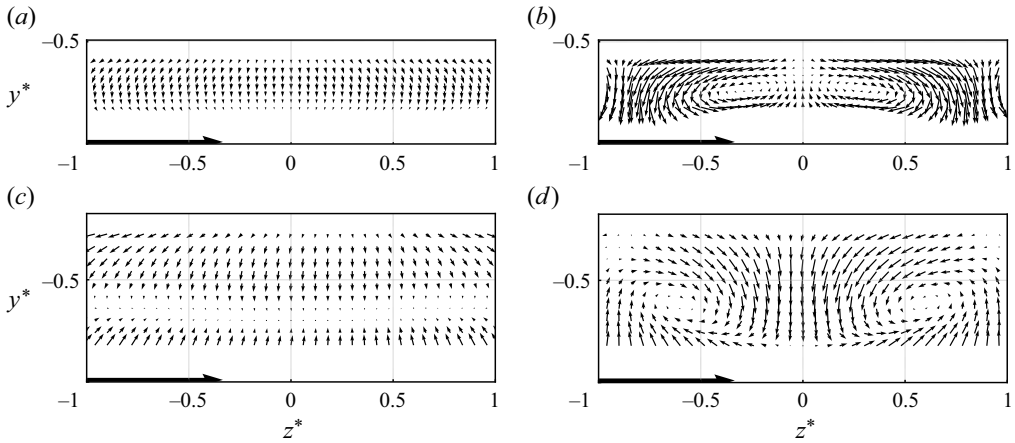


Figure 5. Time-averaged velocity fields on $x=0$ plane. Experimental results with (a) $(\omega, \Psi) = (1.3\pi \text{ rad s}^{-1}, 0.2)$, (b) $(1.73\pi \text{ rad s}^{-1}, 0.2)$, (c) $(0.7\pi \text{ rad s}^{-1}, 0.4)$ and (d) $(0.8\pi \text{ rad s}^{-1}, 0.4)$. The arrows on the frame indicate the wall velocity.

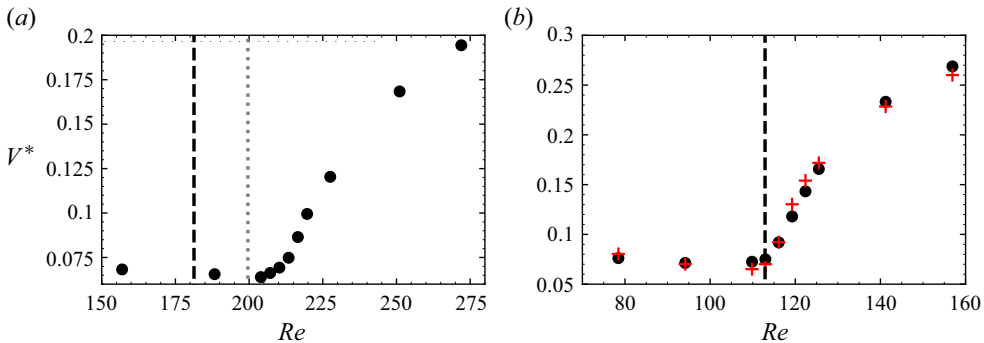


Figure 6. Indicator V^* defined as (3.1) as a function of Re . Experimental results with $L^* = 16$ and (a) $\Psi = 0.2$ and (b) 0.4 . Note that Fr changes with Re . Red crosses in (b) are the DNS results (see § 4.1) under the same condition as in the experiments (table 1). The vertical lines denote the critical Reynolds number Re_c estimated by DNS (see § 4.3) with slip boundary conditions. The dashed and dotted lines are the results with $Fr = 1.81 \times 10^{-2}$ and $Fr = 9.0 \times 10^{-2}$, respectively.

of V^* with Re . The other is the fact that Fr changes with Re in the experiments, since we change the angular velocity for the same container and working fluid. In fact, if we take into account the change in Fr (the red crosses in figure 6b), we can explain the functional form of V^* ; see § 4.1.

It is worth mentioning the size of convection cells. Flow visualizations in figures 3 and 4 show that the size in the axial direction of the convection cells increases with the filling ratio. This observation is important in practice because the limited length of the cylinder restricts the cell size and affects their onsets. We will discuss this issue in §§ 4.2 and 5.2.

In this section, we have experimentally demonstrated the onset of convection cells. In the next section, we numerically investigate the dependence of the onset on various parameters.

Ψ	R (m)	L (m)	ω (rad s ⁻¹)	ρ_l (kg m ⁻³)	μ_l (Pa s)	g (m s ⁻²)	Co	Resolution (n_x, n_y, n_z)
0.4	0.05	0.8	$0.5\pi \leq \omega \leq \pi$	955	0.0478	9.81	0.1	(256, 256, 2048)

Table 1. Numerical conditions for the validation of DNS: Ψ , filling ratio; R , the radius of the cylinder; L , the cylinder length; ω , the magnitude of the angular velocity of the cylinder; ρ_l , liquid density; μ_l , liquid viscosity; g , the magnitude of the gravitational acceleration; $Co = \delta t \Delta / u_{max}$, the Courant number; n_x, n_y and n_z , the grid numbers in x, y and z directions, respectively. We impose no-slip boundary conditions on the end walls.

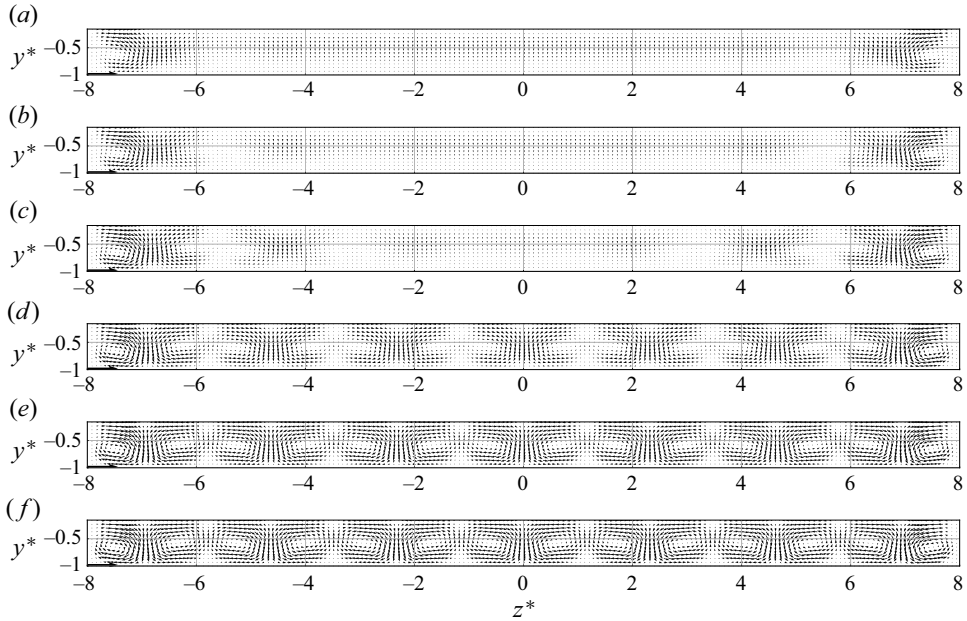


Figure 7. Instantaneous velocity fields on $x = 0$ plane. DNS results, where we impose no-slip boundary conditions on the end walls, with parameters listed in table 1. The angular velocities are (a) 0.5π , (b) 0.6π , (c) 0.7π , (d) 0.8π , (e) 0.9π and (f) π rad s⁻¹. The arrows on the frame indicate the wall velocity.

4. DNS results

4.1. Validation

Before the detailed investigation of the onset of convection cells, we validate the numerical method described in § 2.3. To this, we conduct DNS using the same parameters ($R = 0.05$ m, $L = 0.8$ m, $\rho_l = 955$ kg m⁻³, $\mu_l = 0.0478$ Pa s, $\Psi = 0.4$) as in the experiments shown in § 3. We list the numerical parameters in table 1.

First, we visualize the cross-sectional flow on the $x = 0$ plane in figure 7. We can see that DNS results are consistent with the experimental results shown in figure 4. Specifically, no convection cells exist in a central region of the cylinder for $\omega = 0.6\pi$ rad s⁻¹, while cells are visible for $\omega = \pi$ rad s⁻¹. We can also confirm that the number of convection cells is 14 in both of the experiment and DNS.

To make a more quantitative comparison, we calculate V^* defined as (3.1) and plot the results with red crosses in figure 6(b). It is evident that the DNS results are in good agreement with the experimental data. The critical angular velocity, at which V^* starts to increase, also coincides with the experiments.

Here, we mention the treatment of the solid–gas–liquid contact line in DNS. Specifically, the contact angle is set as 90° (see § 2.2), whereas in the experiments, the wall of the container is wet and therefore there is no contact line. The above validation therefore implies that the numerical treatment of the contact line has little effect on the onset of convection cells in the examined regime.

4.2. Dependence of the cell size on Ψ

As depicted in figures 3 and 4, the axial length λ^* , normalized by R , of a pair of convection cells depends on the filling ratio. Here, we numerically investigate the dependence of λ^* on Ψ . For this purpose, we impose slip boundary conditions on the end walls to simulate flow in an infinitely long cylinder. Table 2(a) shows the numerical conditions; we investigate λ^* in the range $0.052 \leq \Psi \leq 0.9$ under the condition $L^* = 64$ and $Fr = 1.81 \times 10^{-2}$. Here, $\Psi = 0.052$, which corresponds to the case with the liquid height being $0.2R$, is the same filling ratio as in the DNS performed by Romanò *et al.* (2017). To observe the convection cells, we must conduct DNS at a higher Reynolds number than Re_c , which depends on Ψ (see figure 6 for example). This is why we choose Re depending on Ψ as shown in table 2(a): $Re = 200$ for $0.2 \leq \Psi \leq 0.8$, 500 for 0.1 and 0.9 and 700 for 0.052 . We will discuss the detailed Ψ -dependence of Re_c in the next subsection (see figure 12c).

Figure 8 shows the axial velocity component w^* on the vertical plane ($x = 0$ plane). We observe that the number of convection cells varies with Ψ : that is, 72, 52, 39 and 36 with $\Psi = 0.2, 0.4, 0.7$ and 0.9 , respectively. Thus, we conclude that the length λ^* of a pair of convection cells monotonically increases with Ψ (figure 9) and the aspect ratio of a convection cell is approximately constant irrespective of Ψ . Incidentally, our result ($\lambda^* = 0.865$ with $\Psi = 0.052$) is consistent with the result ($\lambda^* = 0.839 \pm 0.01$) of Romanò *et al.* (2017) with the same Ψ .

4.3. Dependence of Re_c on Ψ

In this subsection, we examine the filling-rate dependence of Re_c for the onset of convection cells. Since it requires long computational time to simulate a steady flow in the long cylinder ($L^* = 64$), to reduce them, we conduct DNS of flow in a cylinder with the length λ^* under slip boundary conditions on the end walls. Table 2(b) shows the numerical conditions; as λ^* depends on Ψ (figure 9), we change the number of grids along the z direction for different Ψ .

First, we visualize flow on the $x = 0$ plane to see its dependence on Re for fixed Ψ at 0.4 . Figure 10 shows the results for (a) $Re = 110$ and (b) 115 with $\Psi = 0.4$. The flow has no axial velocity components (figure 10a), while we observe a pair of convection cells at $Re = 115$ (figure 10b), implying that $110 < Re_c < 115$. To clarify the onset of convection cells, we use the indicator (Romanò *et al.* 2017)

$$w_r^* = \max[w^*(0, h_0^* - \delta^*, z^*)], \quad (4.1)$$

which quantifies the intensity of convection cells. Here, δ^* denotes a distance from the liquid–gas interface without rotation, and we set $\delta^* = 0.13$.

We plot the temporally averaged value $\overline{w_r^*}$ as a function of Re for $\Psi = 0.4$ and 0.7 in figure 11(a). For $\Psi = 0.4$, $\overline{w_r^*}$ vanishes at $Re = 110$, and $\overline{w_r^*}$ starts to increase at $Re \approx 114$ as Re increases. This observation implies that the convection cells appear through a supercritical bifurcation. For $\Psi = 0.7$, $\overline{w_r^*}$ starts to increase at $Re \approx 108$, which is smaller than the value for $\Psi = 0.4$. To determine Re_c precisely, we use the feature that if the

Ψ	Re	Fr	L^*	Co	Resolution (n_x, n_y, n_z)
(a) Run 1					
$0.2 \leq \Psi \leq 0.8$	$Re = 200$	1.81×10^{-2}	64	0.1	(256, 256, 4096)
0.1, 0.9	$Re = 500$	1.81×10^{-2}	64	0.1	(256, 256, 4096)
0.052	$Re = 700$	1.81×10^{-2}	64	0.1	(256, 256, 4096)
(b) Run 2					
0.052	$570 \leq Re \leq 590$	1.81×10^{-2}	0.865	0.1	(256, 256, 64)
0.1	$333 \leq Re \leq 340$	1.81×10^{-2}	1.19	0.1	(256, 256, 128)
0.2	$184 \leq Re \leq 188$	1.81×10^{-2}	1.78	0.1	(256, 256, 128)
0.3	$136 \leq Re \leq 140$	1.81×10^{-2}	2.13	0.1	(256, 256, 128)
0.4	$110 \leq Re \leq 135$	1.81×10^{-2}	2.46	0.1	(256, 256, 192)
0.5	$104 \leq Re \leq 108$	1.81×10^{-2}	2.78	0.1	(256, 256, 192)
0.6	$100 \leq Re \leq 104$	1.81×10^{-2}	3.05	0.1	(256, 256, 192)
0.7	$100 \leq Re \leq 120$	1.81×10^{-2}	3.28	0.1	(256, 256, 192)
0.8	$128 \leq Re \leq 132$	1.81×10^{-2}	3.56	0.1	(256, 256, 256)
(c) Run 3					
0.4	$140 \leq Re \leq 150$	1.81×10^{-2}	2.46	0.1	(128, 128, 96)
0.4	$114 \leq Re \leq 116$	1.81×10^{-2}	2.46	0.1	(512, 512, 384)
(d) Run 4					
0.4	$114 \leq Re \leq 116$	1.81×10^{-2}	$2.34 \leq L^* \leq 2.56$	0.1	(256, 256, 192)
0.7	$105 \leq Re \leq 108$	1.81×10^{-2}	$3.12 \leq L^* \leq 3.44$	0.1	(256, 256, 192)
(e) Run 5					
0.2	$201 \leq Re \leq 205$	9.0×10^{-2}	1.78	0.1	(256, 256, 128)
(f) Run 6					
0.9	$244 \leq Re \leq 252$	4.53×10^{-3}	3.56	0.1	(256, 256, 256)
(g) Run 7					
0.2	$182 \leq Re \leq 186$	2.26×10^{-3}	1.78	0.025	(256, 256, 128)
0.2	$182 \leq Re \leq 186$	4.53×10^{-3}	1.78	0.1	(256, 256, 128)
0.2	$182 \leq Re \leq 186$	9.05×10^{-3}	1.78	0.1	(256, 256, 128)
0.2	$194 \leq Re \leq 198$	3.62×10^{-2}	1.78	0.1	(256, 256, 128)
0.2	$188 \leq Re \leq 192$	7.24×10^{-2}	1.78	0.1	(256, 256, 128)
0.4	$113 \leq Re \leq 115$	2.26×10^{-3}	2.46	0.025	(256, 256, 192)
0.4	$113 \leq Re \leq 115$	4.53×10^{-3}	2.46	0.1	(256, 256, 192)
0.4	$114 \leq Re \leq 116$	9.05×10^{-3}	2.46	0.1	(256, 256, 192)
0.4	$115 \leq Re \leq 118$	3.62×10^{-2}	2.46	0.1	(256, 256, 192)
0.4	$118 \leq Re \leq 125$	7.24×10^{-2}	2.46	0.1	(256, 256, 192)
0.7	$104 \leq Re \leq 108$	2.26×10^{-3}	3.28	0.025	(256, 256, 192)
0.7	$104 \leq Re \leq 108$	4.53×10^{-3}	3.28	0.1	(256, 256, 192)
0.7	$104 \leq Re \leq 108$	9.05×10^{-3}	3.28	0.1	(256, 256, 192)
0.7	$106 \leq Re \leq 110$	3.62×10^{-2}	3.28	0.1	(256, 256, 192)
0.7	$107 \leq Re \leq 110$	7.24×10^{-2}	3.28	0.1	(256, 256, 192)
0.193	$188 \leq Re \leq 192$	2.26×10^{-3}	1.78	0.025	(256, 256, 128)
0.386	$115 \leq Re \leq 118$	2.26×10^{-3}	2.46	0.025	(256, 256, 192)
0.688	$104 \leq Re \leq 108$	2.26×10^{-3}	3.28	0.025	(256, 256, 192)

Table 2. Numerical conditions of DNS to investigate (a) the axial wavelength of the most unstable mode in a sufficiently long cylinder, (b) the critical Reynolds number Re_c in the cylinder with the length determined by part (a), (c) resolution convergence, (d) the dependence of Re_c on L^* , (e) consistency with experiments, (f) the bifurcation at $\Psi = 0.9$ and (g) the dependence of Re_c on Fr . We impose slip boundary conditions on the end walls of the cylinder. We list physical and numerical parameters: Ψ , filling ratio; $Re = \rho_l R^2 \omega / \mu_l$, the Reynolds number; $Fr = R \omega^2 / g$, the Froude number; L^* , the cylinder length normalized by R ; $Co = \delta t \Delta / u_{max}$, the Courant number; n_x, n_y and n_z , the grid numbers in x, y and z directions, respectively. In the case with $Fr = 2.26 \times 10^{-3}$, we set $Co = 0.025$ for the sake of numerical stability.

Convection cells in a horizontally rotating cylinder

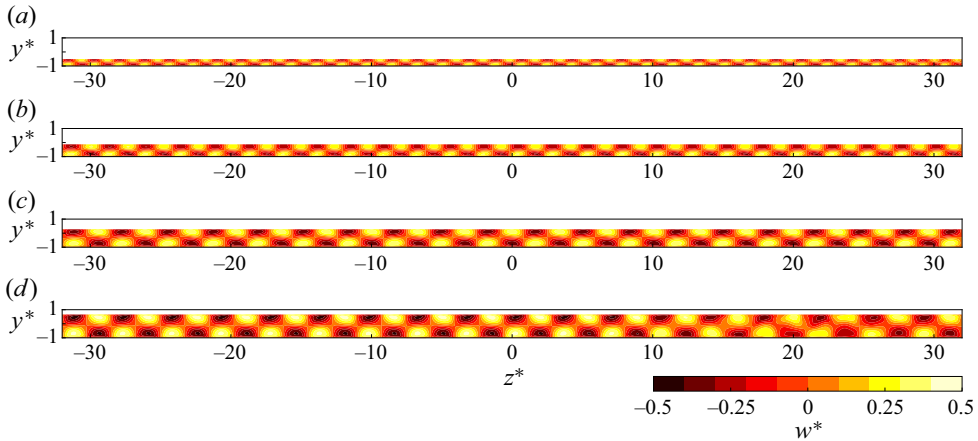


Figure 8. Axial velocity component w^* on $x=0$ plane. DNS (Run 1 in table 2) results under slip boundary conditions on the end walls with (a) $(\Psi, Re) = (0.2, 200)$, (b) $(0.4, 200)$, (c) $(0.7, 200)$ and (d) $(0.9, 500)$. We set $Fr = 1.81 \times 10^{-2}$ for all cases.

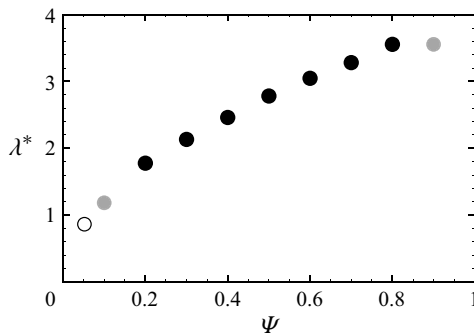


Figure 9. Wavelength λ^* obtained by DNS (Run 1 in table 2) under slip boundary conditions on the end walls with cylinder length $L^* = 64$ as a function of the filling ratio Ψ . The results with $\Psi = 0.052$ (white circle), 0.1, 0.9 (grey) and 0.2–0.8 (black) are obtained at $Re = 700, 500$ and 200, respectively. We set $Fr = 1.81 \times 10^{-2}$ for all the cases.

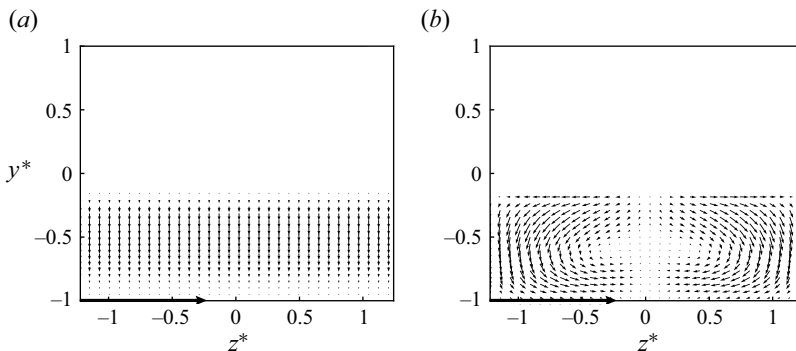


Figure 10. Instantaneous velocity fields on $x=0$ plane. Results of DNS (Run 2 in table 2) under slip boundary conditions on the end walls with $\Psi = 0.4$, $Fr = 1.81 \times 10^{-2}$ and (a) $Re = 110$ and (b) 115. The cylinder length is set as $L^* = \lambda^* = 2.46$. The arrows on the frame indicate the wall velocity.

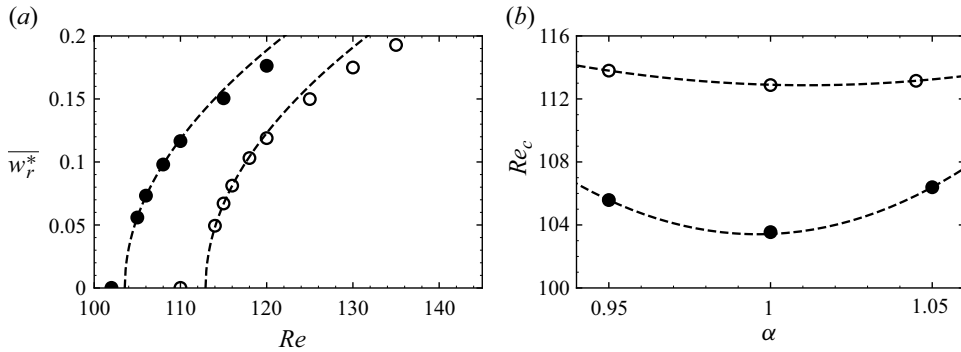


Figure 11. (a) Time-averaged intensity $\overline{w_r^*}$ of convection cells defined as (4.1) as a function of Re for two different values of the filling ratio: \circ , $\Psi = 0.4$; \bullet , 0.7 . The cylinder length L^* is set as λ^* shown in figure 9. Dashed lines represent the fitting by (4.2). Results of DNS (Run 2 in table 2) under slip boundary conditions on the end walls. (b) Relationship between Re_c and $\alpha (= L^*/\lambda^*)$. The symbols are the same as in (a). Dashed lines represent the quadratic function passing three points of (α, Re_c) . Results of DNS (Run 3 in table 2) under slip boundary conditions on the end walls.

	Resolution (n_x, n_y, n_z)	Re_1	Re_2	Re_3	$\overline{w_r^*}(Re_1)$	$\overline{w_r^*}(Re_2)$	$\overline{w_r^*}(Re_3)$	Re_c
DNS_{coarse}	(128, 128, 96)	137	138	140	1.35×10^{-2}	4.79×10^{-2}	8.23×10^{-2}	136.6
DNS_{medium}	(256, 256, 192)	114	115	116	4.84×10^{-2}	6.70×10^{-2}	8.12×10^{-2}	112.9
DNS_{fine}	(512, 512, 384)	114	115	116	6.70×10^{-2}	8.14×10^{-2}	9.35×10^{-2}	111.9

Table 3. Dependence of the critical Reynolds number Re_c on the numerical resolution under the condition $\Psi = 0.4, Fr = 1.81 \times 10^{-2}$ and $L^* = \lambda^*$. We also show the data for fitting by (4.2). For the fitting, we use three values of $\overline{w_r^*}$ at $Re = Re_1, Re_2$ and Re_3 .

convection cells appear through a pitchfork bifurcation, $\overline{w_r^*}$ follows

$$\overline{w_r^*} = c\sqrt{Re - Re_c}, \tag{4.2}$$

where c is a constant. We determine Re_c by fitting three values of $\overline{w_r^*}$ in the range of Re above and nearest Re_c . Dashed lines in figure 11(a) show the fitting curves. Thus, determined critical Reynolds numbers for $\Psi = 0.4$ and 0.7 are 112.9 and 106.4, respectively.

Here, we briefly mention the mesh convergence. We conduct DNS (table 2c) with three different grid numbers: $DNS_{coarse}[(n_x, n_y, n_z) = (128, 128, 96)]$, $DNS_{medium}[(n_x, n_y, n_z) = (256, 256, 192)]$ and $DNS_{fine}[(n_x, n_y, n_z) = (512, 512, 384)]$. Table 3 shows Re_c for the three cases together with Re and $\overline{w_r^*}$, which are used to determine Re_c . Although the value of Re_c obtained by DNS_{coarse} differs significantly from that by DNS_{medium} , Re_c obtained by DNS_{fine} matches the result of DNS_{medium} with only 1% relative difference. Therefore, we conclude that DNS_{medium} is fine enough to estimate Re_c .

Next, we briefly mention the dependence of Re_c on the cylinder length L^* . Recall that, in Run 2 (figure 11a), we set L^* as the axial wavelength λ^* of the cells sustained in a long cylinder ($L^* = 64$). Recall also that we impose slip boundary conditions on the end walls in Run 2 to mimic an infinitely long cylinder. To examine the effects of L^* on Re_c , we set L^* as

$$L^* = \alpha\lambda^*, \tag{4.3}$$

Convection cells in a horizontally rotating cylinder

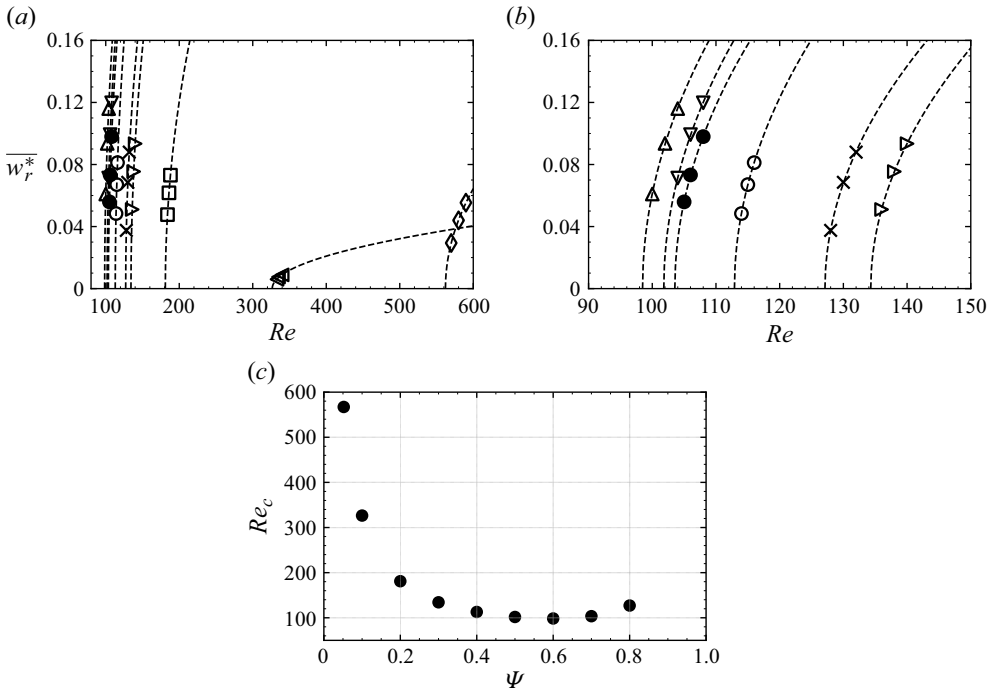


Figure 12. (a) Time-averaged intensity $\overline{w_r^*}$ of convection cells defined as (4.1) as a function of Re . Different symbols denote results with different values of the filling ratio: \diamond , $\Psi = 0.052$; \triangleleft , 0.1; \square , 0.2; \triangleright , 0.3; \circ , 0.4; ∇ , 0.5; \triangle , 0.6; \bullet , 0.7; \times , 0.8. Dashed lines represent the fitting by (4.2). (b) Same as (a) but for the close-up view in the range $90 \leq Re \leq 150$. (c) Re_c as a function of Ψ . Results of DNS (Run 2 in table 2) under slip boundary conditions on the end walls.

where α is a positive coefficient; see table 2(d) for the numerical conditions. Figure 11(b) shows Re_c as a function of α for $\Psi = 0.4$ and 0.7 . We can see that Re_c takes the minimum at approximately $\alpha = 1$ in both cases. This result implies that λ^* approximates the wavelength of the most unstable mode in the infinite-length cylinder.

To investigate the Ψ dependence of Re_c , we apply the above method for various values of Ψ . Figures 12(a) and 12(b) show $\overline{w_r^*}$ as a function of Re . Since $\overline{w_r^*}$ is well fitted by (4.2), we may conclude that the convection cells appear through a pitchfork bifurcation for $0.052 \leq \Psi \leq 0.8$. We also plot Re_c as a function of Ψ in figure 12(c). We can see that Re_c depends on Ψ non-monotonically and it takes minimum at $Re_c \approx 100$ around $0.5 \lesssim \Psi \lesssim 0.7$. Incidentally, we do not show the result for $\Psi = 0.9$ in figure 12(a) because, as will be shown in detail in § 5.1, the convection cells appear through a subcritical bifurcation for $\Psi = 0.9$.

To compare the obtained Re_c with experimental results, we plot vertical dashed lines at Re_c in figures 6(a) and 6(b). For $\Psi = 0.4$, the dashed line well explains the experimental observation that V^* starts to increase as Re increases above a value around Re_c . However, for $\Psi = 0.2$, we see the discrepancy between Re_c and the Reynolds number above which V^* increases. This discrepancy is mainly caused by the difference in Fr . In DNS, we fix Fr to determine Re_c . In contrast, Fr changes with Re in the experiments. Figure 6(a) shows that the cells in the experiments appear at $Re \approx 200$ for $\Psi = 0.2$. In this condition, Fr is 9.0×10^{-2} , which differs significantly from the value (1.81×10^{-2}) in DNS. Therefore, to confirm the consistency between the experiments and DNS, we estimate Re_c with

$Fr = 9.0 \times 10^{-2}$ for $\Psi = 0.2$ by DNS (table 2e). The result ($Re_c \approx 200$) is shown by the vertical grey dotted line in figure 6(a), which well explains the experiments (figure 6a). Incidentally, for $\Psi = 0.4$, the convection cells appear at $Re \approx 110$ (figure 6b), and in this experimental condition, $Fr \approx 2.6 \times 10^{-2}$. In fact, the difference in Fr between DNS and the experiment has little influence on Re_c in this small- Fr range (see figure 18a in § 5.3).

It is worth comparing our results with the previous study (Romanò *et al.* 2017). They showed that the critical Reynolds number was approximately 820 for $\Psi = 0.052$. This is significantly larger than the value ($Re_c = 562$) in our DNS. Although their DNS does not account for interface deformation, it seems not the main cause. To confirm this, we have conducted DNS with sufficiently small Fr ($= 4.53 \times 10^{-3}$); even if we set L^* as done by Romanò *et al.* (2017), the obtained value of the critical Re is approximately 560, which is almost the same as the value (562) for the larger Fr (1.81×10^{-2}). In addition, we have also conducted experiments with the filling ratio as used by Romanò *et al.* (2017), the results (see Appendix A) support the value of Re_c obtained by the present DNS.

5. Discussion

In this section, we investigate three issues. First, we investigate the onset of convection cells for $\Psi \rightarrow 1$. As described in § 4.3, convection cells appear through a pitchfork bifurcation for $0.052 \leq \Psi \leq 0.8$. In contrast, when $\Psi = 1$, the solid-body rotational flow is always stable for any Re . Since the connection of these two regimes is unclear, we investigate flow bifurcation at $\Psi = 0.9$. Second, we investigate the effect of the end walls of the cylindrical container on the flow. Since real containers have end walls, it is important to investigate their effect on the bifurcation. Third, we examine the dependence of Re_c on Fr .

5.1. Onset of convection cells at $\Psi = 0.9$

In the previous section, we have demonstrated that convection cells appeared through a supercritical pitchfork bifurcation for $0.052 \leq \Psi \leq 0.8$. However, regardless of Re , we cannot observe convection cells when the container is filled with liquid (i.e. $\Psi = 1$). This means that the simple two-dimensional rotating flow is linearly unstable for $Re > Re_c(\Psi)$ in the examined range of Ψ (≤ 0.8), whereas it is always stable at $\Psi = 1$. To understand how these two regimes are connected, here we investigate the onset of convection cells and its bifurcation structure at $\Psi = 0.9$.

Table 2(f) shows the numerical conditions, where we set the Froude number as $Fr = 4.53 \times 10^{-3}$. This value is smaller than in DNS shown in the previous section, so that we can further reduce the effect of the oscillation of the liquid–gas interface on the flow. As will be described in § 5.3, this Froude number is sufficiently small to neglect the dependence of Fr on the flow.

We show the bifurcation diagram by using $\overline{w_r^*}$, which is defined as (4.1), in figure 13(a). We can see that the diagram differs from those in the cases with $0.052 \leq \Psi \leq 0.8$ (figures 11a and 12a). We have drawn this diagram (figure 13a) through the following procedure. First, we simulate the steady state with convection cells at $Re = 252$, then gradually decrease Re to plot filled circles. Although the intensity $\overline{w_r^*}$ of convection cells decreases as Re decreases, they still exist for $Re \gtrsim 245$. However, $\overline{w_r^*}$ suddenly drops to zero at $Re = 244$, indicating the disappearance of convection cells. However, when increasing Re from the flow state without convection cells at $Re = 244$, $\overline{w_r^*}$ remains at 0 (open squares in figure 13a) in a range of Re , but $\overline{w_r^*}$ suddenly increases and reaches the

Convection cells in a horizontally rotating cylinder

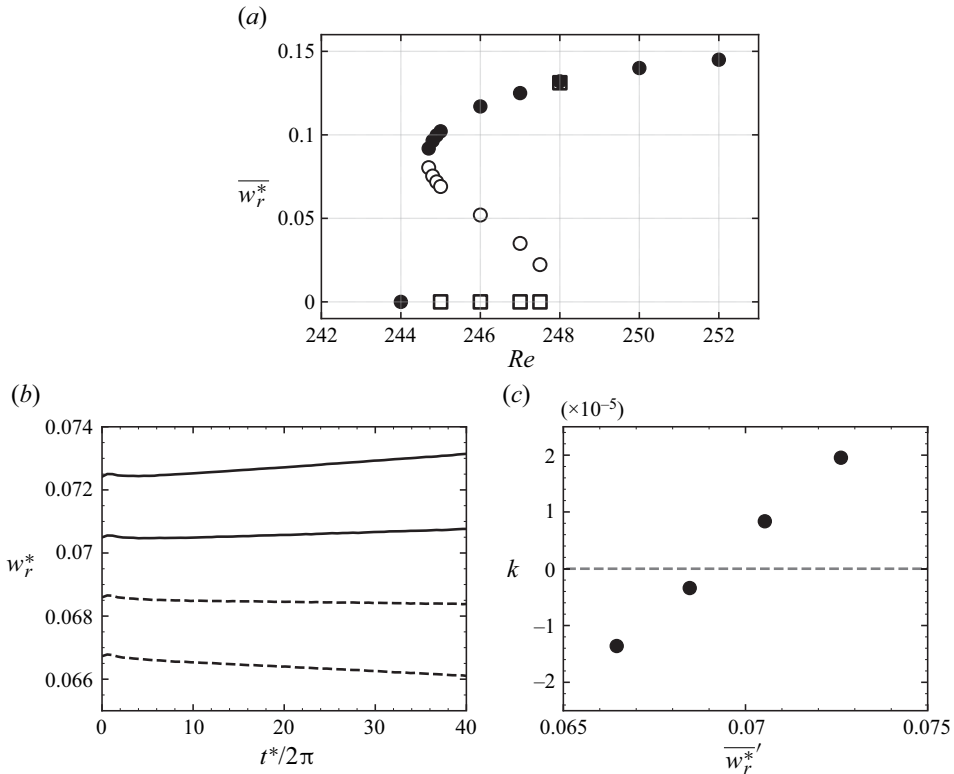


Figure 13. (a) Time-averaged intensity $\overline{w_r^*}$ of convection cells defined as (4.1) as a function of Re . Black-filled circles and open squares are obtained when Re decreases and increases, respectively. Open circles represent the unstable solutions. (b) Temporal evolution of the intensity w_r^* of the convection cells at $Re = 245$ with various initial conditions. Solid and dashed lines indicate the increasing and decreasing functions of time, respectively. (c) Time derivative k of w_r^* in (b) as a function of the time-averaged intensity $\overline{w_r^{*}}$ of convection cells for $20\pi \leq t^* \leq 40\pi$. Results of DNS (Run 6 in table 2) with $\Psi = 0.9$ and $L^* = \lambda^*$ under slip boundary conditions on the end walls.

value (the filled circle) obtained by decreasing Re when the Reynolds number reaches $Re = 248$. This dependence of $\overline{w_r^*}$ on Re implies that the convection cells appear through a subcritical bifurcation at $\Psi = 0.9$ for sufficiently small Fr . It is worth looking at the differences in the convection cells that appear through supercritical and subcritical bifurcations. We compare the two cases in figure 14. Although the velocity fields shown in figures 14(a) and 14(b) appear through supercritical and subcritical bifurcations, respectively, we can observe no quantitative difference in the flow.

As the convection cells appear through a subcritical bifurcation in the case with $\Psi = 0.9$, there are unstable solutions between the upper and lower branches in figure 13(a). To confirm this, we obtain them using a simpler procedure than the conventional ones such as the shooting method.

Here, we explain the method to obtain the unstable solutions at $Re = 245$, for example. First, we construct four initial conditions which have different intensities of convection cells. To obtain them, we simulate flow at $Re = 244$ with the initial condition of the steady state at $Re = 250$. As shown in figure 13(a), since the convection cells cannot be sustained at $Re = 244$, they monotonically decay. Then, we select flow fields at four instances in this decaying process as initial conditions for the runs at $Re = 245$. We plot in figure 13(b)

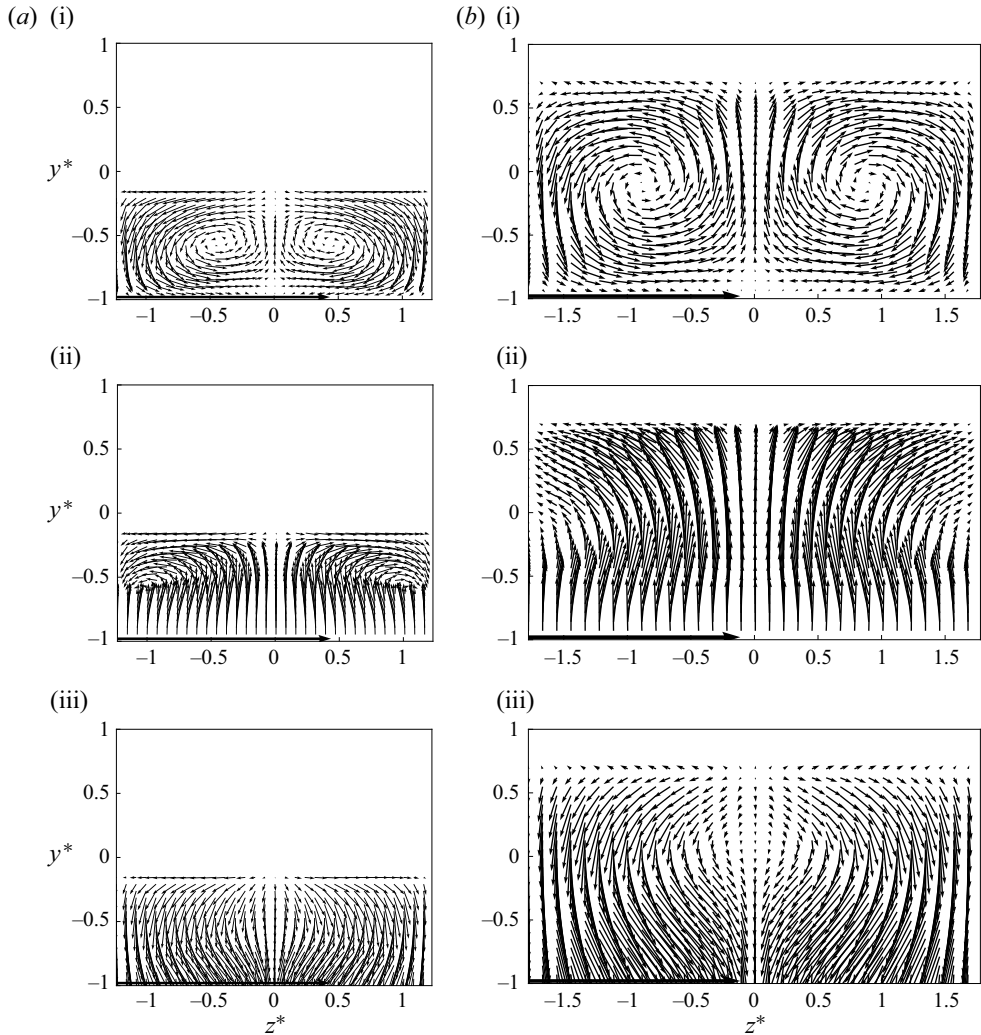


Figure 14. Instantaneous velocity fields just above the onset of the convection cells via (a) supercritical and (b) subcritical bifurcations. We show velocity fields on (i) $x^* = 0$, (ii) -0.25 and (iii) 0.25 planes for (a) $(\Psi, Re) = (0.4, 118)$ and (b) $(0.9, 246)$. DNS (Run 6 and 7 for (b) and (a), respectively, in table 2) results with $Fr = 4.53 \times 10^{-3}$ and $L^* = \lambda^*$ under slip boundary conditions on the end walls.

the evolution of the intensity w_r^* at $Re = 245$ with the four initial conditions. For the initial conditions with $w_r^* > 0.07$, w_r^* increases with time, whereas for those with $w_r^* < 0.07$, w_r^* decreases. Since w_r^* does not increase or decrease on the unstable branch, we can estimate an unstable solution by identifying the point at which the time derivative k of w_r^* becomes zero. We evaluate k by least-square fitting of $w_r^*(t^*)$ between $t^* = 20\pi$ and 40π . Figure 13(c) shows k as a function of $\overline{w_r^*} = (1/20\pi) \int_{40\pi}^{20\pi} w_r^*(t^*) dt^*$. The value of k increases monotonically with $\overline{w_r^*}$, and $k \approx 0$ at $\overline{w_r^*} \approx 0.069$. We estimate $\overline{w_r^*}$ for $k = 0$ by the linear interpolation between two data points at approximately $k = 0$. We plot $\overline{w_r^*}$ for $k = 0$, corresponding to unstable solutions in the range $244.7 \leq Re \leq 247.5$ in

Ψ	Re	Fr	L^*	Co	Resolution (n_x, n_y, n_z)
(a) Run 8					
0.4	$60 \leq Re \leq 200$	1.81×10^{-2}	2.46	0.1	(256, 256, 256)
0.4	$60 \leq Re \leq 200$	1.81×10^{-2}	4.92	0.1	(256, 256, 512)
0.4	$60 \leq Re \leq 200$	1.81×10^{-2}	7.38	0.1	(256, 256, 768)
0.7	$60 \leq Re \leq 200$	1.81×10^{-2}	3.28	0.1	(256, 256, 256)
0.7	$60 \leq Re \leq 200$	1.81×10^{-2}	6.56	0.1	(256, 256, 512)
0.7	$60 \leq Re \leq 200$	1.81×10^{-2}	9.84	0.1	(256, 256, 768)
(b) Run 9					
0.4	$Re = 200$	1.81×10^{-2}	$1.23 \leq L^* \leq 3.69$	0.1	(256, 256, 256)
0.4	$Re = 200$	1.81×10^{-2}	$4.18 \leq L^* \leq 6.15$	0.1	(256, 256, 512)
0.4	$Re = 200$	1.81×10^{-2}	$6.65 \leq L^* \leq 8.12$	0.1	(256, 256, 768)
0.7	$Re = 200$	1.81×10^{-2}	$1.64 \leq L^* \leq 4.92$	0.1	(256, 256, 256)
0.7	$Re = 200$	1.81×10^{-2}	$5.58 \leq L^* \leq 8.20$	0.1	(256, 256, 512)
0.7	$Re = 200$	1.81×10^{-2}	$8.86 \leq L^* \leq 10.8$	0.1	(256, 256, 768)

Table 4. Numerical conditions of DNS to investigate effects of (a) the end walls and (b) the cylinder length on the onset of convection cells. We set no-slip boundary conditions on the end walls.

figure 13(a) with open circles. Thus, from figure 13(a), we conclude that convection cells appear through a subcritical bifurcation at $\Psi = 0.9$.

We have shown the overall bifurcation structures (i.e. the supercritical pitchfork bifurcation for $\Psi \leq 0.8$ and the subcritical bifurcation at $\Psi = 0.9$) of the present system. To obtain a more detailed understanding of the bifurcation, in particular, in the range $0.8 < \Psi < 0.9$, further investigation by linear stability analysis is required, which we leave for a future study. Incidentally, we do not experimentally observe the subcritical bifurcation for $\Psi = 0.9$ due to the effect of the end walls.

5.2. The effect of end walls on the convection cells

In § 4, we investigate flow in the cylinder under the slip boundary conditions on the end walls. This was intended to simulate flow in an infinitely long cylinder. However, since the cylinder’s length is finite in practice, we investigate, in this subsection, the influence of the end walls on the onset of the convection cells by imposing no-slip boundary conditions on the walls.

Table 4(a) shows numerical conditions for this purpose. We examine the onset of convection cells in a finite-length cylinder with two different values of the filling ratio: $\Psi = 0.4$ and 0.7. First, we investigate the dependence of flow on the cylinder length L^* and the Reynolds number Re . More concretely, in each case of the filling ratios, we set L^* as $\alpha\lambda^*$ with α being 1, 2 and 3, where λ^* is the normalized wavenumber corresponding to the most unstable mode in the infinitely long cylinder.

We define the indicator as

$$E_{axis} = \overline{\langle w^{*2} \rangle}, \tag{5.1}$$

of the axial flow intensity to quantify the effects of L^* and Re on the flow. Here, $\langle \cdot \rangle$ denotes the volume average weighted by ϕ_l . We plot E_{axis} as a function of Re for $\Psi = 0.4$ and 0.7 in figures 15(a) and 15(b), respectively. In both cases of Ψ , we observe, irrespective of α , that E_{axis} increases monotonically with Re . We can also notice that the dependence of E_{axis} on Re approaches the case under slip boundary condition (§ 4.3) as α increases. This tendency

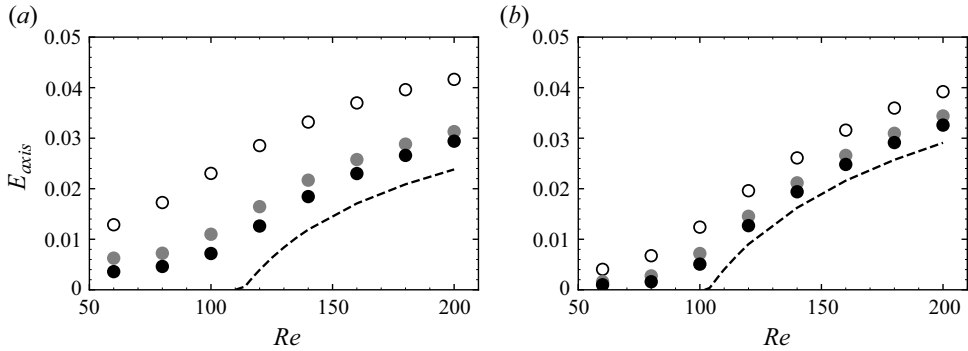


Figure 15. Indicator E_{axis} defined as (5.1) of the magnitude of the axial velocity as a function of Re at $Fr = 1.81 \times 10^{-2}$. The filling ratios are (a) $\Psi = 0.4$ and (b) 0.7 . Different symbols denote results for different cylinder lengths: white, $\alpha = 1$; grey, 2; black, 3. Dashed lines denote the result for $\alpha = 1$ but with slip boundary conditions on the end walls. Results of DNS Run 8, where we impose no-slip boundary conditions on the end walls, in table 4.

is independent of Ψ and implies that the presence of the no-slip end walls makes the pitchfork bifurcation imperfect. In fact, the imperfect pitchfork bifurcation approaches the perfect one as L^* increases because the influence of end walls becomes smaller. Note that we consider the cases with integer α . If α is a non-integer, the dependence of the E_{axis} - Re curve approaches non-monotonically to the dashed line as α increases. It might be worth comparing the present results with those for cavity flow because Blohm & Kuhlmann (2002) experimentally showed that convection cells in a two-sided lid-driven cavity also appeared through an imperfect pitchfork bifurcation.

Next, we investigate the influence of L^* on the flow at fixed Reynolds number ($Re = 200$) and Froude number ($Fr = 1.81 \times 10^{-2}$); the other numerical conditions are listed in table 4(b). Recall that under this condition, convection cells appear because $Re > Re_c$ for $\Psi = 0.4$ and 0.7 and $Fr = 1.81 \times 10^{-2}$ (see figure 12c). First, we visualize flow in figure 16 for $\Psi = 0.7$ on the $x = 0$ plane to demonstrate the dependence of flow on L^* . We observe that the flow strongly depends on α . When α is an integer (figure 16b,d,e), we observe convection cells, and the number of pairs of cells is equal to α . In contrast, when $\alpha = 0.7$ and 1.5 , we do not observe any cells. This observation implies that the cylinder length significantly affects the intensity of convection cells. To more qualitatively understand the dependence of the intensity of convection cells on the cylinder length, we plot E_{axis} as a function of α in figure 17 for $\Psi = 0.4$ and 0.7 . In both cases of Ψ , E_{axis} exhibits non-monotonic dependence on α , and E_{axis} has local maxima when α is close to an integer. This observation implies that the length L^* of the container is appropriate when it is an integer multiple of λ^* to sustain the convection cells. It also implies that the optimal length is independent of the boundary condition on the end walls. Recall that results in figure 17 are obtained under no-slip boundary conditions, whereas those in figure 11 are under the slip boundary conditions.

The results obtained in this subsection may be valuable for designing mixers that use these convection cells. For rapid mixing, we should select L^* as an integer multiple of λ^* . For instance, Varley, Markaki & Brooks (2017) conducted experiments to investigate the relationship between liquid flow in a partially filled cylindrical container and cell culture efficiency. Although they did not observe convection cells probably because of the unoptimized cylinder length, their conclusions might differ if they used a cylinder with different L^* . Since we can generate desirable flow by appropriately setting the cylinder

Convection cells in a horizontally rotating cylinder

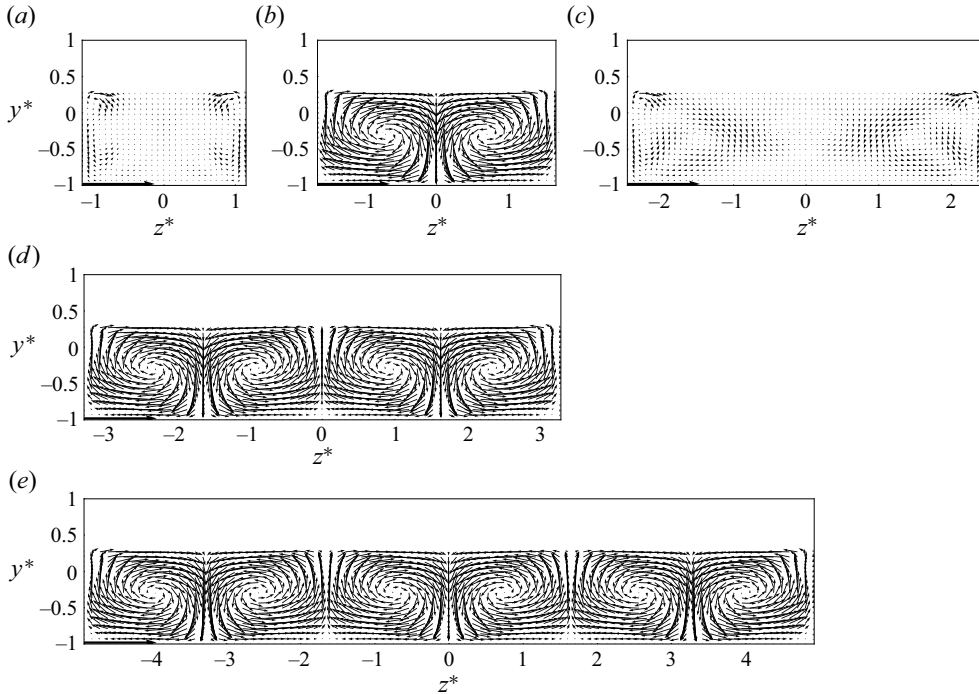


Figure 16. Instantaneous velocity fields on $x = 0$ plane with various cylinder lengths $L^* = \alpha\lambda^*$ at $Re = 200$ under the condition $\Psi = 0.7$ and $Fr = 1.81 \times 10^{-2}$. We impose no-slip boundary conditions on the end walls. Results of DNS (Run 9 in table 4) for (a) $\alpha = 0.7$, (b) 1, (c) 1.5, (d) 2 and (e) 3. The arrows on the frame indicate the wall velocity.

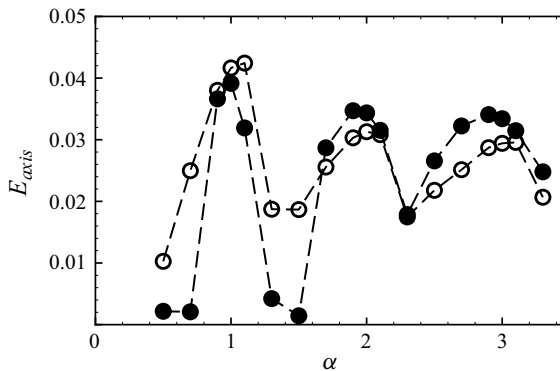


Figure 17. Indicator E_{axis} defined as (5.1) of the magnitude of the axial velocity as a function of $\alpha (= L^*/\lambda^*)$ with $Fr = 1.81 \times 10^{-2}$ and $Re = 200$. The symbols are the same as in figure 11(a). Results of DNS (Run 9 in table 4) under no-slip boundary conditions on the end walls.

length, filling ratio and angular velocity, this system has potential for mixing devices in various applications. In particular, this system may be useful in bioengineering such as cell culture, which requires precise control of flow.

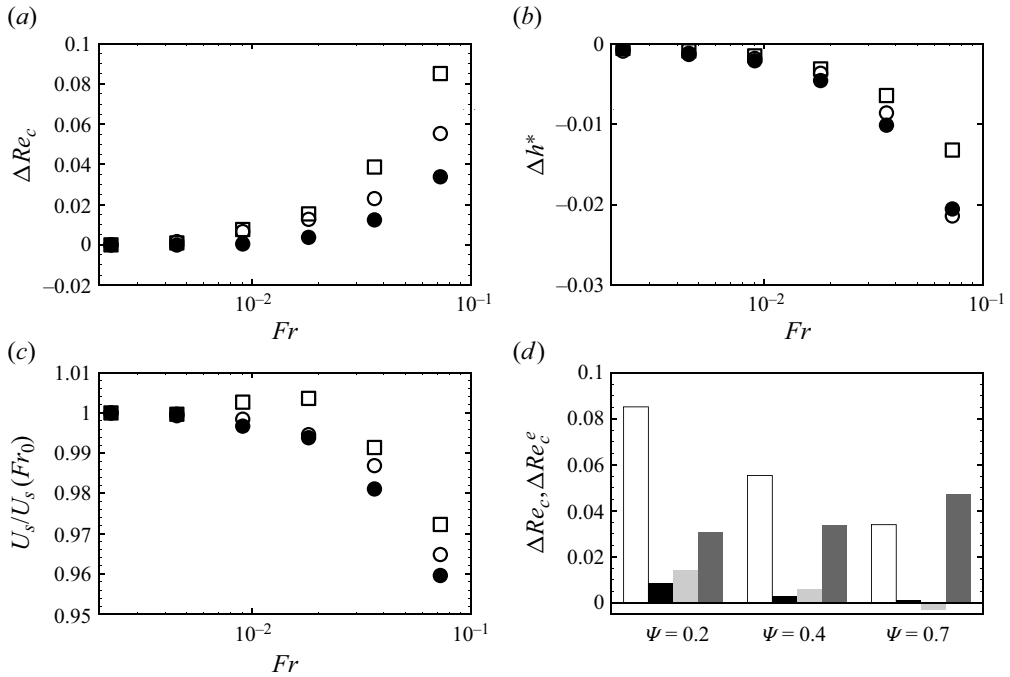


Figure 18. (a) Relative difference ΔRe_c defined as (5.2) of Re_c as a function of Fr . (b) Variation of liquid height Δh^* defined as (5.3) at the centre of the cylinder as a function of Fr . (c) Magnitude of circulation velocity U_s defined as the second equation in (5.4) as a function of Fr . The symbols in panels (a), (b) and (c) are the same as in figure 12(a). (d) Relative differences of the critical Reynolds number at $Fr = 2.26 \times 10^{-3}$ and 7.24×10^{-2} . Different colours of charts denote the result with different definitions of the relative differences: white, the relative difference defined as (5.2); black, both Re^e and Ψ^e are considered; light grey, only Re^e is considered; dark grey, only Ψ^e is considered. These results are obtained by DNS (Run 7 in table 2) with $L^* = \lambda^*$ under slip boundary conditions on the end walls.

5.3. Dependence of Re_c on Fr

In § 4, we have discussed Re_c for a single value of Fr (i.e. 1.81×10^{-2}). In this subsection, we investigate the dependence of Re_c on Fr . Since the objective of the present study is to clarify the onset of convection cells in the liquid-pool regime, we investigate the Fr dependence of Re_c in a small- Fr range, $2.26 \times 10^{-3} (= Fr_0) \leq Fr \leq 7.24 \times 10^{-2} (= Fr_1)$ for each of three filling ratios, $\Psi = 0.2, 0.4$ and 0.7 (table 2g).

Using the method described in § 4.3, we identify Re_c for each combination of Fr and Ψ to clarify the relative increase,

$$\Delta Re_c(Fr, \Psi; Fr_0, \Psi) = \frac{Re_c(Fr, \Psi) - Re_c(Fr_0, \Psi)}{Re_c(Fr_0, \Psi)}, \quad (5.2)$$

from the value at the reference Froude number Fr_0 . Figure 18(a) shows ΔRe_c as a function of Fr for $\Psi = 0.2, 0.4$ and 0.7 . We observe that as Fr increases, ΔRe_c increases for all the examined Ψ , though ΔRe_c is negligibly small for $Fr \lesssim 4 \times 10^{-3}$. This implies that the flow does not significantly depend on Fr in the small- Fr range. We also observe that ΔRe_c in a large- Fr range is larger for smaller Ψ .

We now explain the observed Fr dependence of Re_c by introducing the effective filling ratio Ψ^e and the effective Reynolds number Re^e .

First, we examine the dependence of Ψ^e on Fr . Here, we define Ψ^e by using the liquid height at the centre of the cylinder. Since the container's motion lifts the liquid more easily for larger Fr , the liquid height in a central region decreases for large Fr . To qualify this change, we define

$$\Delta h^* = \overline{h^*} - h_0^*, \tag{5.3}$$

where h^* is the y^* -coordinate satisfying $\phi_l(0, y^*, 0) = 0.5$. We examine flow at Re slightly lower than Re_c to discuss the Fr dependence of Re_c on Fr . Since the flow at $Re (< Re_c)$ is two-dimensional, we conduct two-dimensional simulations to estimate Δh^* . Figure 18(b) shows the estimated variation Δh^* as a function of Fr . We can see that Δh^* and therefore Ψ^e decrease monotonically as Fr increases. We emphasize that Ψ^e differs depending on Fr even if Ψ is the same.

Second, we examine the Fr dependence of Re^e , which we define as

$$Re^e = \rho_l U_s R / \mu_l \quad \text{with } U_s = \langle u^2 + v^2 \rangle^{1/2}. \tag{5.4}$$

It is known that the deformation of the interface affects the circulation velocity in the liquid phase (Terrington, Hourigan & Thompson 2020). Hence, Re^e depends on Fr because of interface deformations for large Fr . Figure 18(c) shows U_s , which is estimated by the two-dimensional simulations, as a function of Fr . We can see that U_s , and therefore Re^e , depend on Fr at any Ψ . Therefore, Re^e differs for the different value of Fr even if Re is the same.

We are ready to explain the Fr dependence of Re_c by using Re^e and Ψ^e . More concretely, we show that Ψ^e determines Re_c^e even when Fr is significantly different. To show this, we need to set two conditions where Ψ^e is common, but Fr is significantly different. However, since we cannot prescribe Ψ^e , we use the numerical observation that Ψ^e is almost the same as Ψ for sufficiently small Fr (figure 18b). Figure 19 shows the construction of the two sets of parameters such that Fr is significantly different but Ψ^e is almost common. The first set of parameters is $Fr = Fr_1$ and Ψ (figure 19a). Under this condition, we conduct DNS to obtain $\Psi^e(Fr_1, \Psi)$, $Re_c(Fr_1, \Psi)$ and $Re_c^e(Fr_1, \Psi)$. Note that $\Psi \gg \Psi^e(Fr_1, \Psi)$ because Fr_1 is sufficiently large (figure 19a). The second set is $Fr = Fr_0$ and $\Psi = \Psi^e(Fr_1, \Psi)$ (figure 19b). Since Fr_0 is sufficiently small, $\Psi^e(Fr_0) \approx \Psi^e(Fr_1)$. Then, we obtain, by DNS, $Re_c(Fr_0, \Psi^e(Fr_1, \Psi))$ and $Re_c^e(Fr_0, \Psi^e(Fr_1, \Psi))$. Thus, we can obtain the critical Reynolds numbers, Re_c and Re_c^e , at two different parameter sets (Fr_1, Ψ) and $(Fr_0, \Psi^e(Fr_1, \Psi))$. Note that $\Psi \gg \Psi^e(Fr_1, \Psi)$ and $Fr_1 \gg Fr_0$, but Ψ^e is almost common for these two parameter sets.

We confirm our hypothesis that Re_c^e is determined by Ψ^e in three cases of Ψ : 0.2, 0.4 and 0.7. To this, we define

$$\Delta Re_c^e(Fr_1, \Psi; Fr_0, \Psi_0) = \frac{Re_c^e(Fr_1, \Psi) - Re_c^e(Fr_0, \Psi_0)}{Re_c^e(Fr_0, \Psi_0)}. \tag{5.5}$$

White charts in figure 18(d) show $\Delta Re_c(Fr_1, \Psi; Fr_0, \Psi)$ and black ones show $\Delta Re_c^e(Fr_1, \Psi; Fr_0, \Psi^e(Fr_1, \Psi))$. It is notable that the latter is significantly smaller than the former for all the three cases of Ψ . This means that the dependence of Re_c on Fr is explained by Ψ^e and Re^e .

We emphasize that it is crucial to consider both of Re^e and Ψ^e . To demonstrate this, we show the relative differences when considering only Re^e (i.e. $\Delta Re_c^e(Fr_1, \Psi; Fr_0, \Psi)$) or Ψ^e (i.e. $\Delta Re_c(Fr_1, \Psi; Fr_0, \Psi^e(Fr_1, \Psi))$) in figure 18(d). It is evident that these are larger than $\Delta Re_c^e(Fr_1, \Psi; Fr_0, \Psi^e(Fr_1, \Psi))$. Furthermore, in the case of $\Psi = 0.7$, the relative difference when considering only Ψ^e exceeds the original one. These results conclude the necessity of considering both Re^e and Ψ^e to understand the dependence of Re_c on Fr .

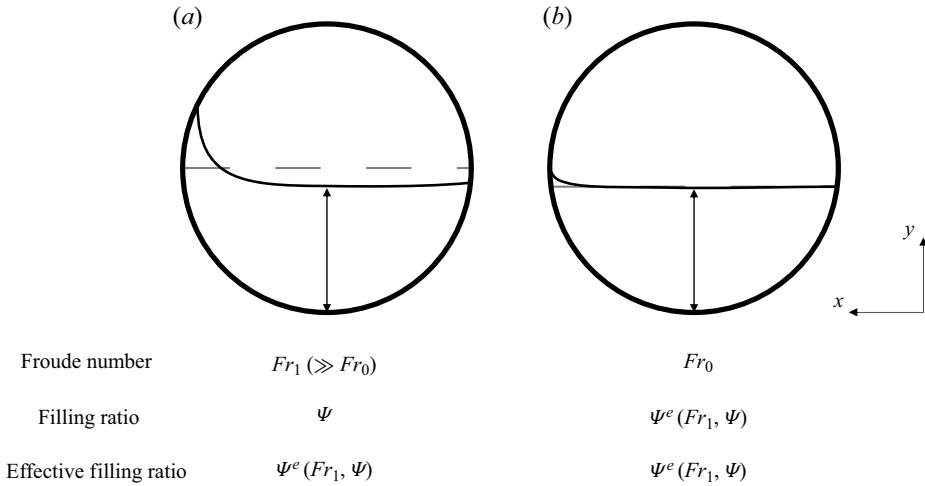


Figure 19. Schematics of the liquid–gas interface with two sets of parameters (a) $(Fr, \Psi) = (Fr_1, \Psi)$ and (b) $(Fr_0, \Psi^e (Fr_1, \Psi))$ such that Fr is significantly different but Ψ^e is almost common. Solid circles indicate the cylindrical walls. Solid and dashed lines represent the liquid–gas interfaces with and without rotation, respectively. Since Fr_1 is sufficiently large, $\Psi \gg \Psi^e (Fr_1, \Psi)$, whereas since Fr_0 is sufficiently small, $\Psi \approx \Psi^e (Fr_1, \Psi)$. Arrows represent the liquid height at the centre of the cylinder with a rotation, whose lengths in (a) and (b) are almost the same.

6. Conclusions

Convection cells can be sustained in liquid phase in a constantly rotating cylinder which is partially filled with liquid (figure 1). We have investigated this canonical flow phenomenon in detail by experiments and DNS.

First, we have demonstrated the onset of convection cells by experiments using a long ($L^* = L/R = 16$) cylindrical container (figure 2). When the angular velocity is small enough, we do not observe the convection cells, but they are visible for a larger angular velocity (figures 3 and 4). To identify the onset of the convection cells, we have quantified the intensity of convection cells by using the data obtained by PIV (figure 5) as a function of Re (figure 6). We can observe flow transition around a certain Reynolds number Re_c , which depends on the filling ratio Ψ . To systematically investigate the onset of convection cells, we conduct DNS of two-phase flow in the container, which has been carefully validated by comparing with experimental results (figures 6 and 7). Then, we have addressed the following five issues: (i) the axial size of the cells; (ii) the dependence of the critical Reynolds number on the filling ratio and aspect ratio of the cylinder in the relatively low- Ψ range; (iii) bifurcation structures in relatively high- Ψ range; (iv) effects of the no-slip end walls on Re_c and the cell size and (v) the weak dependence of Re_c on Fr .

Concerning the first issue, the axial wavelength λ^* normalized by R of the sustained convective cells is longer for larger filling ratio Ψ . This tendency is qualitatively evident in experiments (figures 3 and 4) and qualitatively shown by DNS of flows in a sufficiently long cylinder ($L^* = 64$) with sufficiently small $Fr (= 1.81 \times 10^{-2})$ at sufficiently high Re (figures 8 and 9).

Concerning the second issue, we have numerically investigated the onset of the convection cells by changing Re with Fr fixed at a small value (1.81×10^{-2}). Although ideally, we should conduct DNS with a sufficiently long cylinder like in figures 8 and 9, to reduce the computational cost, we conduct DNS under slip boundary conditions

on the end walls (figure 10) with setting the cylinder length L^* as the wavelength λ^* obtained by DNS with the long cylinder. Then, we have shown that the convection cells appear through a pitchfork bifurcation (figure 11a). Using this knowledge, we determine the critical Reynolds number Re_c by fitting the data with (4.2). Concerning the dependence of Re_c on the cylinder length, we have shown that Re_c for slightly different cylinder lengths takes a minimum value at $L^* = \lambda^*$ (figure 11b). This may imply that the obtained Re_c with a finite length λ^* of cylinder indeed corresponds to the critical value for a sufficiently long cylinder.

The critical Reynolds number Re_c non-monotonically depends on Ψ (figure 12c) for fixed Fr . The critical values Re_c obtained by DNS and experiments are consistent for $\Psi = 0.4$ (figure 6a). Although there seems to be a discrepancy for $\Psi = 0.2$ (figure 6b), it is explained by the difference in Fr (§ 4.3).

Concerning the third issue on the bifurcation structures, although the convection cells appear through a pitchfork bifurcation for $0.052 \leq \Psi \leq 0.8$, solid-body rotational flow is always stable irrespective of Re at $\Psi = 1$. To clarify the connection between these two regimes, we have investigated the onset of convection cells for $\Psi = 0.9$ (figure 13), where we observe a hysteresis loop. This means that the convection cells appear through a subcritical bifurcation at $\Psi = 0.9$. We have also determined the unstable branch (open circles in figure 13a) between the upper (flow with convection cells) and lower (without the cells) stable branches using the simple method explained in § 5.1.

Concerning the fourth issue on the effect of end walls, we have investigated their effect on the onset of the convection cells. Our investigation shows the following two points. First, the presence of no-slip end walls makes the pitchfork bifurcation imperfect (figure 15). This figure shows that the intensity E_{axis} of axial velocity increases monotonically as Re increases in all the cases of cylinder length irrespective of Ψ , and that the E_{axis} - Re curves approach, as L^* increases, the result obtained with slip boundary conditions on the end walls. Second, the optimal container length to sustain convection cells seems independent of the boundary conditions on the end walls. Figure 17 shows that the length L^* of the container is appropriate when it is an integer multiple of λ^* to sustain the convection cells. This is consistent with the visualization of flow on the $x = 0$ plane (figure 16).

Concerning the fifth issue, we recall that the focus of the present study is on the liquid-pool regime. This is why we have dealt with the small- Fr range, for which the deformation of the liquid-gas interface is negligibly small. However, as shown in § 5.3, Re_c does depend on Fr (figure 18a), though the dependence is weak. We have shown that Re_c increases monotonically as Fr increases for all Ψ . Two primary factors contribute to the Fr dependence of Re_c . First, the liquid height in a central region changes with Fr (figure 18b). Consequently, the effective filling ratio Ψ^e also changes. Second, the circulation velocity and therefore the effective Reynolds number Re^e defined as (5.4) are affected by Fr (figure 18c). To substantiate these considerations, we have shown that the effective critical Reynolds number Re_c^e is determined by Ψ^e (figure 18d).

In the present paper, we have not mentioned the mechanism by which convection cells emerge. To understand it, we have to carefully investigate flow structures near the liquid-gas interface because previous studies (Thoroddsen & Mahadevan 1997; Thoroddsen & Tan 2004) showed instability along the stagnation line on the interface. The knowledge on the instability in cavity flows, which are driven by the motion of one or two sidewalls, may be also helpful. Albensoeder, Kuhlmann & Rath (2001) claimed that three-dimensional structures appeared due to centrifugal instability when the one sidewall moves, while Kuhlmann, Wanschura & Rath (1997) concluded that they were

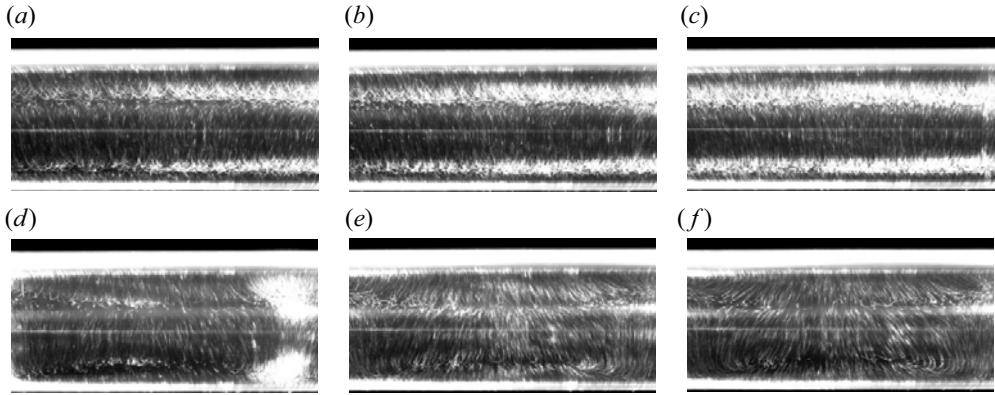


Figure 20. Experimental results with the filling ratio $\Psi = 0.052$. Pathlines on $x = 0$ plane are visualized. The angular velocities are (a) 1.15, (b) 1.26, (c) 1.36, (d) 1.47, (e) 1.57 and (f) 1.67 rad s^{-1} , which correspond to (a) $Re = 480$, (b) 525, (c) 567, (d) 610, (e) 654 and (f) 698, respectively.

due to elliptical instability when both the two sidewalls move. Since our system may also experience one of these instabilities, it is an important future study to conduct linear stability analysis to reveal the mechanism sustaining the convection cells.

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Appendix

We conduct experiments with $\Psi = 0.052$, which is the same filling ratio as used by Romanò *et al.* (2017). The experimental set-up and methods are the same as in § 2.2 except for the working fluid and tracer particles. If we used silicone oil with a kinematic viscosity of $50 \text{ mm}^2 \text{ s}^{-1}$ as in the other cases ($\Psi = 0.2$ and 0.4), Fr could become large at approximately Re_c ($Fr \approx 1.3$ at $Re = 820$) and the deformation of the liquid–gas interface could not be neglected. Therefore, we use silicone oil with a kinematic viscosity of $6 \text{ mm}^2 \text{ s}^{-1}$ (Shinetsu-Silicone KF96-A6CS) instead. In this case, the liquid–gas interface keeps almost horizontal, since Fr is sufficiently small ($Fr \approx 0.02$ at $Re = 820$). Accordingly, since the viscosity of liquid is smaller and the angular velocity is also smaller in the transitional range (e.g. 1.15 rad s^{-1} for the smallest value of the angular velocity), tracer particles easily settle. Hence, we seed nylon powder with a smaller diameter (approximately $20 \text{ }\mu\text{m}$).

Convection cells in a horizontally rotating cylinder

Since the liquid height is too short to conduct PIV, we only show visualization results in figure 20. For $1.15 \text{ rad s}^{-1} \leq \omega \leq 1.36 \text{ rad s}^{-1}$ ($480 \leq Re \leq 567$) in figure 20(a–c), we observe no convection cells, whereas we observe them for $1.47 \text{ rad s}^{-1} \leq \omega \leq 1.67 \text{ rad s}^{-1}$ ($610 \leq Re \leq 698$) in figure 20(d–f). This implies that the convection cells appear at approximately $567 \lesssim Re_c \lesssim 610$, which is consistent with the present DNS result ($Re_c = 562$) for $\Psi = 0.052$ with sufficiently small Fr .

REFERENCES

- ALBADAWI, A., DONOGHUE, D.B., ROBINSON, A.J., MURRAY, D.B. & DELAURÉ, Y.M.C. 2013 Influence of surface tension implementation in volume of fluid and coupled volume of fluid with level set methods for bubble growth and detachment. *Intl J. Multiphase Flow* **53**, 11–28.
- ALBENSOEDER, S., KUHLMANN, H.C. & RATH, H.J. 2001 Three-dimensional centrifugal-flow instabilities in the lid-driven-cavity problem. *Phys. Fluids* **13**, 121–135.
- ARDEKANI, M.N., AL ASMAR, L., PICANO, F. & BRANDT, L. 2018 Numerical study of heat transfer in laminar and turbulent pipe flow with finite-size spherical particles. *Intl J. Heat Fluid Flow* **71**, 189–199.
- ASHMORE, J., HOSOI, A.E. & STONE, H.A. 2003 The effect of surface tension on rimming flows in a partially filled rotating cylinder. *J. Fluid Mech.* **479**, 65–98.
- BALMER, R.T. 1970 The hygrocyt—a stability phenomenon in continuum mechanics. *Nature* **227**, 600–601.
- BENILOV, E.S., BENILOV, M.S. & KOPTOVA, N. 2008 Steady rimming flows with surface tension. *J. Fluid Mech.* **597**, 91–118.
- BENJAMIN, T.B. & PATHAK, S.K. 1987 Cellular flows of a viscous liquid that partly fills a horizontal rotating cylinder. *J. Fluid Mech.* **183**, 399–420.
- BLOHM, C.H. & KUHLMANN, H.C. 2002 The two-sided lid-driven cavity: experiments on stationary and time-dependent flows. *J. Fluid Mech.* **450**, 67–95.
- BOHÁČEK, J., KHARICHA, A., LUDWIG, A. & WU, M. 2015 An approximate riemann solver for shallow water equations and heat advection in horizontal centrifugal casting. *Appl. Maths Comput.* **267**, 179–194.
- CHATTERJEE, S., SUGILAL, G. & PRABHU, S.V. 2019 Heat transfer in a partially filled rotary evaporator. *Intl J. Therm. Sci.* **142**, 407–421.
- CHEN, P.J., TSAI, Y.T., LIU, T.J. & WU, P.Y. 2007 Low volume fraction rimming flow in a rotating horizontal cylinder. *Phys. Fluids* **19**, 128107.
- DAWEDEIT, C., *et al.* 2012 Coating functional sol-gel films inside horizontally-rotating cylinders by rimming flow/state. *J. Sol-Gel Sci. Tech.* **65**, 170–177.
- DE VITA, F., DE LILLO, F., VERZICCO, R. & ONORATO, M. 2021 A fully Eulerian solver for the simulation of multiphase flows with solid bodies: application to surface gravity waves. *J. Comput. Phys.* **438**, 110355.
- DODD, M.S. & FERRANTE, A. 2014 A fast pressure-correction method for incompressible two-fluid flows. *J. Comput. Phys.* **273**, 416–434.
- FRANTZIS, C. & GRIGORIADIS, D.G.E. 2019 An efficient method for two-fluid incompressible flows appropriate for the immersed boundary method. *J. Comput. Phys.* **376**, 28–53.
- GHOSH, A.K. 2011 Fundamentals of paper drying—theory and application from industrial perspective. In *Evaporation, Condensation and Heat transfer* (ed. A. Ahsan), pp. 535–582. InTech.
- GOTO, S., *et al.* 2023 Precessing cylinder as high-shear-rate mixer: application to emulsification. *Phys. Fluids* **35**, 035139.
- GOTO, S., SHIMIZU, M. & KAWAHARA, G. 2014 Turbulent mixing in a precessing sphere. *Phys. Fluids* **26**, 115106.
- HIRT, C.W. & NICHOLS, B.D. 1981 Volume of fluid (vof) method for the dynamics of free boundaries. *J. Comput. Phys.* **39**, 201–225.
- HOSOI, A.E. & MAHADEVAN, L. 1999 Axial instability of a free-surface front in a partially filled horizontal rotating cylinder. *Phys. Fluids* **11**, 97–106.
- HUBBE, M.A. 2021 Energy efficiency challenges in pulp and paper manufacturing: a tutorial review. *BioResources* **16**, 8567–8639.
- JOHNSON, R.E. 1988 Steady-state coating flows inside a rotating horizontal cylinder. *J. Fluid Mech.* **190**, 321–342.
- KAJISHIMA, T., TAKIGUCHI, S., HAMASAKI, H. & MIYAKE, Y. 2001 Turbulence structure of particle-laden flow in a vertical plane channel due to vortex shedding. *JSME Intl J. Ser. B* **44**, 526–535.
- KAKIMPA, B., MORVAN, H. & HIBBERD, S. 2016 The depth-averaged numerical simulation of laminar thin-film flows with capillary waves. *Trans. ASME: J. Engng Gas Turbines Power* **138**, 112501.

- KEERTHIPRASAD, K.S., MURALI, M.S., MUKUNDA, P.G. & MAJUMDAR, S. 2011 Numerical simulation and cold modeling experiments on centrifugal casting. *Metall. Trans. B* **42**, 144–155.
- KIM, T., CHUNG, J., KIM, D.Y., MOON, J.H., LEE, S., CHO, M., LEE, S.H. & LEE, S. 2016 Design and optimization of rotating triboelectric nanogenerator by water electrification and inertia. *Nano Energy* **27**, 340–351.
- KOZLOV, V. & POLEZHAJEV, D. 2015 Flow patterns in a rotating horizontal cylinder partially filled with liquid. *Phys. Rev. E* **92**, 013016.
- KUHLMANN, H.C., WANSCHURA, M. & RATH, H.J. 1997 Flow in two-sided lid-driven cavities: non-uniqueness, instabilities, and cellular structures. *J. Fluid Mech.* **336**, 267–299.
- LIPSON, S.G. 2001 Periodic banding in crystallization from rotating supersaturated solutions. *J. Phys.: Condens. Matter* **13**, 5001.
- MAJEED, H.A., PEREIRA, V.B., WANG, T., D'AMICO, J.V. & KONONCHEK, C. 2022 Investigation of two-phase rimming flow and heat transfer inside rotational paper cylinder dryers using three multiphase computational models. *J. Therm. Sci. Engng Appl.* **14**, 081002.
- MCCBRIDE, D., HUMPHREYS, N.J., CROFT, T.N., GREEN, N.R., CROSS, M. & WITHEY, P. 2013 Complex free surface flows in centrifugal casting: computational modelling and validation experiments. *Comput. Fluids* **82**, 63–72.
- MELO, F. 1993 Localized states in a film-dragging experiment. *Phys. Rev. E* **48**, 2704.
- MENEKSE, O., WOOD, J.V. & RILEY, D.S. 2006 Investigation of Fe₂O₃–Al and Cr₂O₃–Al reactions using a high speed video camera. *Mater. Sci. Tech.* **22**, 199–205.
- MEUNIER, P. 2020 Geoinspired soft mixers. *J. Fluid Mech.* **903**, A15.
- NICHOLSON, J.M.P., POWER, H., TAMMISOLA, O., HIBBERD, S. & KAY, E.D. 2019 Fluid dynamics of the slip boundary condition for isothermal rimming flow with moderate inertial effects. *Phys. Fluids* **31**, 033602.
- PEREIRA, M., VALENZUELA, R.C. & VALENZUELA, M.A. 2010 Experimental evaluation and modeling of condensate effects in dryer cylinders. *IEEE Trans. Ind. Applics.* **46**, 1321–1331.
- PHILLIPS, O.M. 1960 Centrifugal waves. *J. Fluid Mech.* **7**, 340–352.
- ROMANÒ, F., HAJISHARIFI, A. & KUHLMANN, H.C. 2017 Cellular flow in a partially filled rotating drum: regular and chaotic advection. *J. Fluid Mech.* **825**, 631–650.
- SADEGHI, H., DIOSADY, L. & BLAIS, B. 2022 A computational fluid dynamics study on rimming flow in a rotating cylinder. *Phys. Fluids* **34**, 063304.
- SEIDEN, G. & THOMAS, P.J. 2011 Complexity, segregation, and pattern formation in rotating-drum flows. *Rev. Mod. Phys.* **83**, 1323.
- SEIDEN, G., UNGARISH, M. & LIPSON, S.G. 2005 Banding of suspended particles in a rotating fluid-filled horizontal cylinder. *Phys. Rev. E* **72**, 021407.
- STROGATZ, S.H. 2018 *Nonlinear Dynamics and Chaos with Student Solutions Manual: With Applications to Physics, Biology, Chemistry, and Engineering*. CRC.
- SUN, X. & SAKAI, M. 2016 Numerical simulation of two-phase flows in complex geometries by using the volume-of-fluid/immersed-boundary method. *Chem. Engng Sci.* **139**, 221–240.
- SUSSMAN, M. 2001 *An Adaptive Mesh Algorithm for Free Surface Flows in General Geometries, Adaptive Method of lines* (ed. A. Vande Wouwer, P. Saucez & W.E. Scheisser), p. 207. Chapman and Hall/CRC.
- SUSSMAN, M., SMERKA, P. & OSHER, S. 1994 A level set approach for computing solutions to incompressible two-phase flow. *J. Comput. Phys.* **114**, 146–159.
- TERRINGTON, S.J., HOURIGAN, K. & THOMPSON, M.C. 2020 The generation and conservation of vorticity: deforming interfaces and boundaries in two-dimensional flows. *J. Fluid Mech.* **890**, A5.
- THORODDSEN, S.T. & MAHADEVAN, L. 1997 Experimental study of coating flows in a partially-filled horizontally rotating cylinder. *Exp. Fluids* **23**, 1–13.
- THORODDSEN, S.T. & TAN, Y.K. 2004 Free-surface entrainment into a rimming flow containing surfactants. *Phys. Fluids* **16**, L13–L16.
- TIRUMKUDULU, M. & ACRIVOS, A. 2001 Coating flows within a rotating horizontal cylinder: lubrication analysis, numerical computations, and experimental measurements. *Phys. Fluids* **13**, 14–19.
- VARLEY, M.C., MARKAKI, A.E. & BROOKS, R.A. 2017 Effect of rotation on scaffold motion and cell growth in rotating bioreactors. *Tissue Engng A* **23**, 522–534.
- WATANABE, D. & GOTO, S. 2022 Simple bladeless mixer with liquid–gas interface. *Flow* **2**, E28.
- WILLEMS, G.P., KROES, J.P., GOLOMBOK, M., VAN ESCH, B.P.M., VAN KEMENADE, H.P. & BROUWERS, J.J.H. 2010 Performance of a novel rotating gas-liquid separator. *J. Fluids Engng* **132**, 031301.
- YIH, C.S. 1960 Instability of a rotating liquid film with a free surface. *Proc. R. Soc. Lond. A* **258**, 63–89.

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- YOKOI, K. 2007 Efficient implementation of thinc scheme: a simple and practical smoothed VOF algorithm. *J. Comput. Phys.* **226**, 1985–2002.
- YOKOI, K. 2013 A practical numerical framework for free surface flows based on CLSVOF method, multi-moment methods and density-scaled CSF model: numerical simulations of droplet splashing. *J. Comput. Phys.* **232**, 252–271.